

Higher-order approximate solutions of fractional stochastic point kinetics equations in nuclear reactor dynamics

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Abstract Stochastic point kinetics equations (SPKEs) are a system of Itô stochastic differential equations whose solution has been obtained by higher-order approximation. In this study, a fractional model of SPKEs has been analyzed. The efficiency of the proposed higher-order approximation scheme has been discussed in the results section. The solutions of SPKEs in the presence of Newtonian temperature feedback have also been provided to further discuss the physical behavior of the fractional model.

Keywords Fractional stochastic point reactor kinetics equations · Fractional calculus · Higher-order approximation · Caputo derivative · Neutron population

1 Introduction

Stochastic point kinetics equations (SPKEs) are a system of coupled nonlinear stochastic differential equations (SDEs) [1] and are important in nuclear engineering. The SPKEs model a system of Itô SDEs, specifically, neutron population and delayed neutron precursors. The physical dynamical system has been established to be a population process, and techniques have been employed by Hayes and Allen [2] to transform deterministic point kinetics equations into a system of SDEs. The fractional diffusion model is normally applied to large variations of neutron cross

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sections, which preclude the use of classical neutron diffusion equations [3–6]. Various approximation methods have been developed to improve the control of processes in the nuclear reactor.

In recent developments, dynamic, multiphysics phenomena face many challenges regarding accurate numerical schemes, resulting in severe computational requirements. An approach to reduce the severe computational requirements of standard low-order simulations is to employ higher-order formulations. In the hierarchy of highorder methods, compact schemes represent an attractive choice for reducing dispersion and anisotropy errors.

Nowak et al. [7] presented the numerical solutions of a fractional neutron point kinetics model for a nuclear reactor. Numerical solutions of SPKEs by implementing stochastic piecewise continuous approximation (PCA) have been obtained by Hayes and Allen [2], which provided a very succinct idea about the randomness of neutron density and precursor concentrations. Saha Ray [8] showed that Euler–Maruyama (EM) and Taylor 1.5 strong order numerical schemes are well-founded estimators compared with stochastic PCA. Saha Ray and Patra [9] applied the Grunwald–Letnikov definition of fractional derivative for solving SPKEs. Nahla and Edress [10] showed the efficiency of analytical exponential model (AEM) for obtaining solutions of SPKEs.

In our present work, we demonstrate the fractional numerical method for obtaining the mean neutron population for various reactivities. In Sect. 2, we introduce the fractional stochastic nonlinear point reactor kinetics equations (SNPKE). The fractional Itô SDE for NPKEs is obtained using the central limit theorem. In Sect. 3, we discuss the higher-order approximation method for Caputo derivative, and in Sect. 4, we discuss its application. In

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Sect. 5, we discuss the obtained numerical solutions for various reactivities.

2 Framework of fractional SNPKE

We now introduce an elementary definition before stating the central limit theorem.

Definition 2.1 Let \bar{X}_M be the sample mean of M independent samples X_1, \ldots, X_M of a random variable X such that

$$\bar{X}_M = \frac{1}{M}(X_1 + \dots + X_M), \quad X_M^* = \sqrt{M}(\bar{X}_M - \mu),$$

where μ is the mean and σ^2 is the variance for each independent and identically distributed real-valued random variables X_j .

Theorem 2.1 (Central Limit Theorem) If each random variable X_j has a finite second moment with $\operatorname{Var} X_j = \sigma^2$, the distribution of \overline{X}_M converges to that of a Gaussian random variable with mean μ and variance $\frac{\sigma^2}{M}$. Thus, X_M^* converges in distribution to $Z \sim N(0, \sigma^2)$.

The fractional Itô SDE for NPKEs with temperature feedback effects [11-15] obtained from the central limit theorem can be written as follows [16]:

$${}_{0}^{C}D_{t}^{\alpha}\boldsymbol{\Psi}(t) = \boldsymbol{A}(t)\boldsymbol{\Psi}(t) + \boldsymbol{Q} + \boldsymbol{B}^{\frac{1}{2}}(t)\frac{\mathrm{d}\boldsymbol{W}(t)}{\mathrm{d}t}, \qquad (2.1)$$

where α is the fractional order of the derivative and $0 < \alpha \le 1$,

$$\Psi(t) = \begin{pmatrix} N(t) \\ C_1(t) \\ C_2(t) \\ \vdots \\ C_m(t) \end{pmatrix},$$

$$\boldsymbol{W}(t) = \begin{pmatrix} W_0(t) \\ W_1(t) \\ W_2(t) \\ \vdots \\ W_m(t) \end{pmatrix},$$

and $Q = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 0 \end{pmatrix}$. Here, *m* is the total number of delayed

neutron groups and $W_0(t)$, $W_1(t)$, $W_2(t)$,..., $W_m(t)$ are standard Wiener processes as defined in [8], N(t) is the

neutron population, and $C_i(t)$ is the precursor concentration of *i*-group of delayed neutrons.

The coefficient matrix A(t) is represented in the fol-

lowing form =
$$\begin{pmatrix} W_0(t) \\ W_1(t) \\ W_2(t) \\ \vdots \\ W_m(t) \end{pmatrix}$$

$$A(t) = \begin{pmatrix} \frac{\rho - \beta}{l} & \lambda_1 & \lambda_2 & \dots & \lambda_m \\ \frac{\beta_1}{l} & -\lambda_1 & 0 & \dots & 0 \\ \frac{\beta_2}{l} & 0 & -\lambda_2 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \frac{\beta_m}{l} & 0 & 0 & \dots & -\lambda_m \end{pmatrix},$$
(2.2)

where ρ is the total reactivity, $\beta = \sum_{i=1}^{m} \beta_i$ is the total fraction of delayed neutrons, β_i is the fraction and λ_i is the decay constant of *i*-group of delayed neutrons, and *l* is the prompt neutron generation time.

The covariance matrix $\boldsymbol{B}(t)$, which is evaluated in Ref. [16], is represented as follows:

$$\boldsymbol{B}(t) = \begin{pmatrix} \mu_0(t) & -\mu_1(t) & -\mu_2(t) & \dots & -\mu_m(t) \\ -\mu_1(t) & \mu_1(t) & 0 & \dots & 0 \\ -\mu_2(t) & 0 & \mu_2(t) & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -\mu_m(t) & 0 & 0 & \dots & \mu_m(t) \end{pmatrix},$$
(2.3)

where $\mu_0(t) = \left(\frac{\rho+\beta}{l}\right)N(t) - \sum_{i=1}^m \lambda_i C_i(t), \ \mu_i(t) = \frac{\beta_i}{l}N(t) - \lambda_i C_i(t),$ and i=1,2,3,...,m.

3 Higher-order approximation scheme

3.1 Fractional calculus

The Caputo derivative operator for $\alpha \in (0,1)$ is defined as follows:

$${}_{0}^{C}D_{t}^{\alpha}f(t) = \frac{1}{\Gamma(1-\alpha)}\int_{0}^{t}(t-s)^{-\alpha}f'(s)\mathrm{d}s,$$

in which $\Gamma(\cdot)$ is the Euler gamma function.

In this paper, a $(3 - \alpha)^{\text{th}}$ order scheme for Caputo derivative ${}_{0}^{C}D_{t}^{\alpha}\Psi(t)$ with $\alpha \in (0, 1)$ has been discussed for obtaining the solutions of fractional SNPKEs. Let $0 = t_{0} < t_{1} < \cdots < t_{M} = T$ and $t_{n} = t_{0} + n\tau$ be the equidistant discretized times with $\tau = \Delta_{n} = \frac{(T-t_{0})}{M}$ for $M \in \mathbb{Z}$ such that

 $\tau \in (0, 1)$. Now, using the Taylor expansion to $\Psi'(s)$, $\Psi(t_{i-1})$, and $\Psi(t_{i+1})$ at point $t = t_i (0 \le i < n)$, we get

$$\begin{split} \Psi'(s) &= \Psi'(t_i) + \Psi''(t_i)(s-t_i) + \frac{\Psi'''(t_i)}{2!}(s-t_i)^2 \\ &+ O((s-t_i)^3), \quad s \in (t_i, t_{i+1}), \\ \Psi'(t_i) &= \frac{\Psi(t_{i+1}) - \Psi(t_{i-1})}{2\tau} - \frac{\Psi'''(t_i)}{3!}\tau^2 + O(\tau^4), \text{ and} \\ \Psi''(t_i) &= \frac{\Psi(t_{i+1}) - 2\Psi(t_i) + \Psi(t_{i-1})}{\tau^2} - \frac{\Psi^{(4)}(t_i)}{12}\tau^2 \end{split}$$

Hence, we can obtain the following:

$$\begin{split} \Psi'(s) &= \frac{\Psi(t_{i+1}) - \Psi(t_{i-1})}{2\tau} + \frac{\Psi(t_{i+1}) - 2\Psi(t_i) + \Psi(t_{i-1})}{\tau^2} \\ &(s - t_i) - \frac{\Psi'''(t_i)}{3!}\tau^2 + \frac{\Psi'''(t_i)}{2!}(s - t_i)^2 \\ &+ O((s - t_i)^3), \quad 0 < s - t_i < \tau. \end{split}$$

Therefore, the Caputo derivative can be discretized as

$$\begin{split} {}_{0}^{C}D_{t}^{\alpha}\Psi(t)|_{t=t_{n}} &= \frac{1}{\Gamma(1-\alpha)} \int_{0}^{t_{n}} (t_{n}-s)^{-\alpha}\Psi'(s)\mathrm{d}s \\ &= \frac{1}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} \int_{t_{i}}^{t_{i+1}} (t_{n}-s)^{-\alpha}\Psi'(s)\mathrm{d}s \\ &= \frac{1}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} \int_{t_{i}}^{t_{i+1}} (t_{n}-s)^{-\alpha} \\ &\left[\frac{\Psi(t_{i+1}) - \Psi(t_{i-1})}{2\tau} + \frac{\Psi(t_{i+1}) - 2\Psi(t_{i}) + \Psi(t_{i-1})}{\tau^{2}} (s-t_{i}) \right. \\ &\left. - \frac{\Psi'''(t_{i})}{3!} \tau^{2} + \frac{\Psi'''(t_{i})}{2!} (s-t_{i})^{2} \right] \mathrm{d}s + O(\tau^{3}) \\ &= \frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \sum_{i=0}^{n-1} \left[w_{1,n-i}(\Psi_{i+1} - \Psi_{i-1}) \right. \\ &\left. + w_{2,n-i}(\Psi_{i+1} - 2\Psi_{i} + \Psi_{i-1}) \right] + r^{n} \end{split}$$

where n = 1, 2, ..., M and τ^n is the truncation error.

Therefore, the Caputo derivative has the following numerical approximation [17]:

$${}^{C}_{0}D^{\alpha}_{t_{n}}\Psi(t_{n}) = \frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \sum_{i=0}^{n-1} \times [w_{1,n-i}(\Psi_{i+1} - \Psi_{i-1}) + w_{2,n-i}(\Psi_{i+1} - 2\Psi_{i} + \Psi_{i-1})] + O(\tau^{3-\alpha}),$$
(3.1)

where $0 < \alpha < 1$, $w_{1,n-i} = \frac{2-\alpha}{2} [(n-i)^{1-\alpha} - (n-i-1)^{1-\alpha}]$, $w_{2,n-i} = (n-i)^{2-\alpha} - (n-i-1)^{2-\alpha} - (2-\alpha)(n-i-1)^{1-\alpha}$, and r^n is the truncation error in the following form:

$$r^{n} = \frac{1}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} \int_{t_{i}}^{t_{i+1}} (t_{n}-s)^{-\alpha} [-C_{\Psi}\tau^{2} + 3C_{\Psi}(s-t_{i})^{2}] ds + O(\tau^{3}),$$
(3.2)

where $C_{\Psi} = \frac{\Psi'''(t_i)}{3!}$ is a constant. The right-hand side of Eq. (3.2) can be expressed as follows:

$$\begin{aligned} \frac{1}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} \int_{t_i}^{t_{i+1}} (t_n - s)^{-\alpha} \\ & [-C_{\Psi}\tau^2 + 3C_{\Psi}(s - t_i)^2] ds + O(\tau^3) \\ & = \frac{C_{\Psi}}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} (I_1 + 3I_2), \end{aligned}$$

where

$$\begin{split} I_1 &= -\int_{t_n}^{t_{n+1}} (t_n - s)^{-\alpha} \tau^2 \mathrm{d}s \\ &= \frac{\tau^{3-\alpha}}{1-\alpha} [(n-i-1)^{1-\alpha} - (n-i)^{1-\alpha}], \\ I_2 &= \int_{t_n}^{t_{n+1}} (t_n - s)^{-\alpha} (s-t_i)^2 \mathrm{d}s \\ &= \frac{\tau^{3-\alpha}}{1-\alpha} (n-i-1)^{1-\alpha} - \frac{2\tau^{3-\alpha}}{(1-\alpha)(2-\alpha)} (n-i-1)^{2-\alpha} \\ &- \frac{2\tau^{3-\alpha}}{(1-\alpha)(2-\alpha)(3-\alpha)} [(n-i-1)^{3-\alpha} - (n-i)^{3-\alpha}]. \\ &= \frac{\tau^{3-\alpha}}{(1-\alpha)(2-\alpha)(3-\alpha)} [(n-i-1)^{3-\alpha} - (n-i)^{3-\alpha}]. \end{split}$$

Therefore,

$$\frac{C_{\Psi}}{\Gamma(1-\alpha)} \sum_{i=0}^{n-1} (I_1 + .3I_2) = \\ \begin{cases} -n^{1-\alpha} - 3[(n-1)^{1-\alpha} + \dots + 2^{1-\alpha} + 1] \\ -\frac{6}{2-\alpha}[(n-1)^{3-\alpha} + \dots + 2^{3-\alpha} + 1]. \\ +\frac{6}{(2-\alpha)(3-\alpha)}n^{3-\alpha} \end{cases}.$$

Let

$$S(n) = -3\sum_{i=1}^{n-1} i^{1-\alpha} - \frac{6}{2-\alpha} \sum_{i=1}^{n-1} i^{2-\alpha} + \frac{6}{(2-\alpha)(3-\alpha)} n^{3-\alpha} - n^{1-\alpha}$$
$$= \sum_{i=1}^{n-1} a_i, \quad n \ge 1.$$

If n = 1, define $a_0 = s(1) = \frac{6}{(2-\alpha)(3-\alpha)} - 1$. Then, $a_i(i \le 1)$ can be defined as follows:

$$a_{i} = S(i+1) - S(i)$$

= $\frac{6}{(2-\alpha)(3-\alpha)}[(i+1)^{3-\alpha} - i^{3-\alpha}] - \frac{6}{2-\alpha}i^{2-\alpha} - (i+1)^{1-\alpha} - 2i^{1-\alpha}.$

It can be proven that |S(n)| is bounded for $n \ge 1$ [17–19]. This proves that the series $\sum_{i=0}^{\infty} a_i$ converges.

On further simplification, we get:

$${}_{0}^{C}D_{t_{n}}^{\alpha}\Psi(t_{n}) = \frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \left[\Psi_{n}(w_{1,1}+w_{2,1}) + \sum_{i=0}^{n-2} w_{1,n-i}\Psi_{i+1} - \sum_{i=0}^{n-1} w_{1,n-i}\Psi_{i-1} + \sum_{i=0}^{n-2} w_{2,n-i}\Psi_{i+1} + \sum_{i=0}^{n-1} w_{2,n-i}(-2\Psi_{i}+\Psi_{i-1}) \right] + O(\tau^{3-\alpha})$$

$$(3.3)$$

In Eq. (3.2), if i = 0, then $\Psi_{i-1} = \Psi_{-1}$, which lies outside of [0, T]. Various options have been provided to approach Ψ_{-1} . In numerical calculations, the neighboring function values have been used to approximate Ψ_{-1} , that is, $\Psi_{-1} = \Psi(0) - \tau \Psi'(0) + \frac{\tau^2}{2} \Psi''(0) + O(\tau^3)$.

1. When
$$\Psi'(0) = \Psi''(0) = 0$$
, then $\Psi_{-1} = \Psi_0 + O(\tau^3)$;
the convergence order is $O(\tau^{3-\alpha})$.

- 2. When $\Psi'(0) = 0$, $\Psi''(0) \neq 0$, then $\Psi_{-1} = \Psi_0$ $+ \frac{\tau^2}{2} \Psi''(0) + O(\tau^3)$; the convergence order of Eq. (3.1) is $O(\tau^2)$.
- 3. When $\Psi'(0) \neq 0$, then the convergence order is $O(\tau)$.

Table 1 Mean peak values of N(t) for different step reactivities

4 Solution of SPKE by higher-order approximation method

In this section, higher-order approximation to Caputo derivative has been applied to Eq. (2.1) as follows:

$$\frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \left[\Psi_n(w_{1,1}+w_{2,1}) + \sum_{i=0}^{n-2} w_{1,n-i} \Psi_{i+1} - \sum_{i=0}^{n-1} w_{1,n-i} \Psi_{i-1} + \sum_{i=0}^{n-2} w_{2,n-i} \Psi_{i+1} + \sum_{i=0}^{n-1} w_{2,n-i} (-2\Psi_i + \Psi_{i-1}) \right]$$

$$= \mathbf{A}(t) \Psi(t) + \mathbf{Q} + \mathbf{B}^{\frac{1}{2}}(t) \frac{\mathrm{d}\mathbf{W}(t)}{\mathrm{d}t}$$
(4.1)

Therefore, the above expression can be simplified into an explicit numerical scheme as follows:

$$\Psi_{n} = \frac{1}{(w_{1,1} + w_{2,1})} \left(\Gamma(3 - \alpha)\tau^{\alpha} \Big(\boldsymbol{A}(t_{n-1})\Psi_{n-1} + \boldsymbol{Q} + \boldsymbol{B}^{\frac{1}{2}}(t_{n-1})\Delta \boldsymbol{W}(t_{n}) \Big) - \left(\sum_{i=0}^{n-2} w_{1,n-i}\Psi_{i+1} - \sum_{i=0}^{n-1} w_{1,n-i}\Psi_{i-1} + \sum_{i=0}^{n-2} w_{2,n-i}\Psi_{i+1} + \sum_{i=0}^{n-1} w_{2,n-i}(-2\Psi_{i} + \Psi_{i-1}) \right) \right)$$

$$(4.2)$$

where $\Delta W(t_n) = \sqrt{h}S_n$ and n = 1, 2, ..., M with initial condition

$$\Psi(0) = \begin{pmatrix} \frac{N_0}{l\lambda_1} \\ \frac{\beta_2 N_0}{l\lambda_2} \\ \vdots \\ \frac{\beta_I N_0}{l\lambda_m} \end{pmatrix},$$
(4.3)

ρ	$\alpha = 0.96$		$\alpha = 0.98$		$\alpha = 0.99$		EM $\alpha = 1$	Taylor 1.5 strong order $\alpha = 1$ [8]	AEM $\alpha = 1$	ESM $\alpha = 1$	
	Peak	Time (s)	Peak	Time (s)	Peak	Time (s)	Peak	Peak	Peak	Peak	
0.003 0.007	180.796 128.655	0.1 0.001	180.033 128.248	0.095 0.001	180.819 124.113	0.083 0.001	208.6 139.568	199.408 139.569	186.30 134.54	179.93 134.96	



Fig. 1 (Color online) Mean N(t) and two arbitrary sample paths for **a** step reactivity $\rho = 0.003$ and $\alpha = 0.96$, **b** step reactivity $\rho = 0.003$ and $\alpha = 0.99$, **c** step reactivity $\rho = 0.003$ and $\alpha = 0.99$

Table 2 Mean peak values of N(t) for ramp reactivity $\rho = 0.1\beta t$ and different values of fractional order α

a	σ	$\alpha = 0.96$	$\alpha = 0.96$		$\alpha = 0.98$			AEM $\alpha = 1$ [20]	ESM $\alpha = 1$ [10]	
		Peak	Time (s)	Peak	Peak	Peak	Time (s)	Peak	Peak	
$0.1\beta t$	10^{-11}	113.563	0.998	113.275	186.30	113.045	0.1	113.267707	113.116433	



Fig. 2 (Color online) Mean N(t) and two arbitrary sample paths for **a** ramp reactivity $\rho = 0.1\beta t$ and $\alpha = 0.96$, **b** ramp reactivity $\rho = 0.1\beta t$ and $\alpha = 0.99$, **c** ramp reactivity $\rho = 0.1\beta t$ and $\alpha = 0.99$

Table 3 Mean peak values of
$N(t)$ for $\rho_{\rm ex} = 0.5\beta$,
$\rho_{\rm ex} = 0.75\beta$, and $\rho_{\rm ex} = \beta$, b
comparison of mean peak
values of $N(t)$ for $\rho_{\text{ex}} = 0.5\beta$,
$\rho_{\rm ex} = 0.75\beta$, and $\rho_{\rm ex} = \beta$ for
$\alpha = 1$, and $\alpha = 0.98$

ρ_{ex}	$\alpha = 0.96$		$\alpha = 0.98$		$\alpha = 0.99$		
	Peak	Time (s)	Peak	Time (s)	Peak	Time (s)	
(a)							
0.5β	42.6182	28.65	44.789	30.29	45.9708	29.25	
0.75β	159.21	8.875	160.124	8.895	162.99	9.305	
β	801.166	0.985	795.268	1.03	772.893	1.0625	
$\rho_{\rm ex}$	SSFEMM [15	$[\alpha = 1)$	DFMM [15] (<i>α</i> = 1)	$\alpha = 0.98$		
	Peak	Time (s)	Peak	Time (s)	Peak	Time (s)	
(b)							
0.5β	46.4939	28.34	46.2606	27.84	44.789	30.29	
0.75β	163.707	8.795	164.22	8.95	160.124	8.895	
β	760.589	1.065	769.238	1.0575	795.268	1.03	



Fig. 3 (Color online) Mean N(t) and two arbitrary sample paths for **a** step reactivity $\rho_{\text{ex}} = 0.5\beta$ and $\alpha = 0.96$, **b** step reactivity $\rho_{\text{ex}} = 0.75\beta$ and $\alpha = 0.96$, **c** step reactivity $\rho_{\text{ex}} = \beta$ and $\alpha = 0.96$

$$\boldsymbol{S}_{n} = \begin{pmatrix} \boldsymbol{S}_{0_{n}} \\ \boldsymbol{S}_{1_{n}} \\ \boldsymbol{S}_{2_{n}} \\ \vdots \\ \boldsymbol{S}_{m_{n}} \end{pmatrix},$$
(4.4)

where $S_{0_n}, S_{1_n}, S_{2_n}, \dots, S_{m_n}$ are random variables from N(0, 1) with mean equal to 0 and variance equal to 1.



Fig. 4 (Color online) Mean N(t) and two arbitrary sample paths for **a** step reactivity $\rho_{\rm ex} = 0.5\beta$ and $\alpha = 0.98$, **b** step reactivity $\rho_{\rm ex} = 0.75\beta$ and $\alpha = 0.98$, **c** step reactivity $\rho_{\rm ex} = \beta$ and $\alpha = 0.98$

Theorem 4.1 The local truncation error of the scheme is $O(\tau^{3-\alpha})$.

Proof The local truncation error of the higher-order scheme for Eq. (4.2) can be derived as follows:



Fig. 5 (Color online) Mean N(t) and two arbitrary sample paths for **a** step reactivity $\rho_{\text{ex}} = 0.5\beta$ and $\alpha = 0.99$, **b** step reactivity $\rho_{\text{ex}} = 0.75\beta$ and $\alpha = 0.99$, **c** step reactivity $\rho_{\text{ex}} = \beta$ and $\alpha = 0.99$

$$\begin{split} R_{j}^{k} &= \frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \sum_{i=0}^{n-1} \\ & [w_{1,n-i}(\Psi_{i+1}-\Psi_{i-1}) + w_{2,n-i}(\Psi_{i+1}-2\Psi_{i}+\Psi_{i-1})] \\ & - A(t_{n-1})\Psi_{n-1} - Q - B^{\frac{1}{2}}(t_{n-1})\Delta W(t_{n}) \\ &= \frac{\tau^{-\alpha}}{\Gamma(3-\alpha)} \sum_{i=0}^{n-1} \\ & [w_{1,n-i}(\Psi_{i+1}-\Psi_{i-1}) + w_{2,n-i}(\Psi_{i+1}-2\Psi_{i}+\Psi_{i-1})] \\ & - {}_{0}^{C} D_{t_{n}}^{\alpha} \Psi(t_{n}) - A(t_{n-1})(\Psi_{n-1}-\Psi_{n-1}) \\ &= O(\tau^{3-\alpha}). \end{split}$$

5 Numerical results and discussions

Here, the solutions of SPKE (i = 6) have been obtained using higher-order approximation scheme.

5.1 Step reactivity

In this section, the numerical solutions of the fractional stochastic point kinetic model [10] using the following parameters have been obtained: $\lambda_1 = 0.0127 \text{ s}^{-1}$, $\lambda_2 = 0.0317 \text{ s}^{-1}$, $\lambda_3 = 0.115 \text{ s}^{-1}$, $\lambda_4 = 0.311 \text{ s}^{-1}$, $\lambda_5 = 1.4 \text{ s}^{-1}$, $\lambda_6 = 3.87 \text{ s}^{-1}$, $\beta_1 = 0.000266$, $\beta_2 = 0.001491$, $\beta_3 = 0.001316$, $\beta_4 = 0.002849$, $\beta_5 = 0.000896$, $\beta_6 = 0.000182$, $\beta = 0.007$, $l = 2.0 \times 10^{-5}$ s, v = 2.5, and q = 0 with $N(0) = N_0 = 100$ (neutron) and $C_i(0) = \frac{\beta_i N(0)}{l \lambda_i}$.

For different step reactivities, i.e., $\rho = 0.003$ and $\rho = 0.007$, the mean peak values of N(t) with respect to time for fractional orders $\alpha = 0.96$, 0.98, and 0.99 at step size h = 0.001 s and for 500 trials are presented in Table 1. In addition, the results have been compared with those obtained by other methods, namely EM [8], Taylor 1.5 strong order [8], AEM [20], and efficient stochastic model (ESM) [10] with graphical representation in Fig. 1. The solutions of SPKE obtained using the above-discussed fractional scheme have been tabulated to establish the efficiency of the higher-order approximation method.

5.2 Ramp reactivity

The numerical solutions of the fractional SNPKE have been obtained using the same parameters as those in Sect. 5.1. Here, the reactivity can be represented as $\rho = 0.1\beta t$.

For ramp external reactivity, i.e., $\rho = 0.1\beta t$, the mean peak values of N(t) with respect to time for fractional orders $\alpha = 0.96$, 0.98, and 0.99 at step size h = 0.001 s and for 500 trials are listed in Table 2. In addition, the results have been compared with those obtained using other methods, namely AEM [20] and ESM [10] with graphical representation in Fig. 2. The solutions of SPKE obtained using the above-discussed fractional scheme have been tabulated to establish the efficiency of the higher-order approximation method.

5.3 Temperature feedback reactivity

In this section, solutions of fractional stochastic point kinetic model with *i*-group of delayed neutrons (i = 6) in the presence of Newtonian temperature feedback have been obtained using the higher-order approximation method.

Table 4 Mean peak values of N(t) for $\rho_{ex} = 0.1t$ and 0.01t, $\rho(t) = at - \sigma \int_{0}^{t} N(\tau) d\tau$, b comparison of mean peak values of N(t) for $\rho_{ex} = 0.1t$ and 0.01t, $\rho(t) = at - \sigma \int_{0}^{t} N(\tau) d\tau$ for $\alpha = 1$ and $\alpha = 0.98$

			0			0.00						
а	σ		$\alpha = 0.96$			$\alpha = 0.98$				$\alpha = 0.99$		
			Peak		Time (s)	Peak		Time (s)		Peak	Time (s)	
(a)												
0.01	10	$-^{11}$	1.6986	$\Theta E + 10$	1.084	1.76031E -	+ 10	1.103	1	.73211E + 10	1.112	
	10	-13	2.0663	E + 12	1.132	2.18262E -	+ 12	1.151	2	2.13422E + 12	1.161	
0.1	10^{-11}		1.78236E + 11		0.223	1.90873E + 11		0.232	2	2.01965E + 11		
	10^{-13}		2.34211E + 13		0.238	2.37627E + 13		0.248	2	2.41795E + 13	0.252	
а	σ SSFEMM [15] (α =		$\alpha = 1$)	DFMM [15] (α =	= 1) AEM [M [10] ($\alpha = 1$)		$\alpha = 0.98$			
		Peak		Time (s)	Peak	Time (s)	Peak		Time (s)	Peak	Time (s)	
(b)												
0.01	10^{-11}	1.686	04E + 10	1.118	1.69492E + 10	1.118	1.67343	36E + 10	0.854	1.76031E + 10	1.103	
	10^{-13}	2.120	34E + 12	1.169	2.12802E + 12	1.168	2.08253	31E + 12	0.877	2.18262E + 12	1.151	
0.1	10^{-11}	1.888	49E + 11	0.235	1.89642E + 11	0.235	1.79057	77E + 11	0.142	1.90873E + 11	0.232	
	10^{-13}	2.244	48E + 13	0.251	2.26026E + 13	0.251	2.14377	78E + 13	0.150	2.37627E + 13	0.248	

The total reactivity of the reactor in the presence of temperature feedback [21] is represented in the following form:

$$\rho(t) = \rho_{\text{ex}}(t) - \rho_f(t), \quad \rho_f(t) = \sigma \int_0^t N(\tau) d\tau.$$

where $\sigma = \alpha K_c$, $\rho_{ex}(t)$ is the external reactivity, T(t) is the temperature, T_0 is the initial temperature, α is the temperature coefficient, and K_c is the reciprocal of the thermal capacity.

In the interval $[t_k, t_{k+1}]$, the total reactivity can be expressed as follows [15]:

$$\rho(t_k) \approx \rho_{\rm ex}(t_k) - h\sigma \sum_{j=0}^k N(t_j).$$

5.3.1 Step external reactivity

In this section, the numerical solutions of the SPKE of U²³⁵ nuclear reactor [3] using the following parameters have been obtained: $\lambda_1 = 0.0124 \text{ s}^{-1}$, $\lambda_2 = 0.0305 \text{ s}^{-1}$, $\lambda_3 = 0.111 \text{ s}^{-1}$, $\lambda_4 = 0.301 \text{ s}^{-1}$, $\lambda_5 = 1.13 \text{ s}^{-1}$, $\lambda_6 = 3.0 \text{ s}^{-1}$, $\beta_1 = 0.00021$, $\beta_2 = 0.00141$, $\beta_3 = 0.00127$, $\beta_4 = 0.00255$, $\beta_5 = 0.00074$, $\beta_6 = 0.00027$, $\beta = 0.00645$, $l = 5.0 \times 10^{-5} \text{ s}$, $\alpha = 5.0 \times 10^{-5} \text{ K}^{-1}$, and $K_c = 0.05 \text{ K/MW}_{\text{s}}$ with $N(0) = N_0 = 1$ (neutron) and $C_i(0) = \frac{\beta_i N(0)}{L_i}$.

For different step external reactivities, i.e., $\rho_{ex} = 0.5\beta$, $\rho_{ex} = 0.75\beta$, and $\rho_{ex} = \beta$, the mean peak values of N(t) for fractional orders $\alpha = 0.96$, 0.98, and 0.99 and for different step external reactivities 0.5β , 0.75β , and β using 500 trials are presented in Table 3a. These results have been compared with previously obtained results of split-step forward EM method (SSFEMM) and derivative-free Milstein method (DFMM) [15] in Table 3b with graphical representation in Figs. 3, 4, and 5. The solutions of SPKE obtained using the above-discussed fractional scheme have been tabulated to establish the efficiency of the higher-order approximation scheme.

For $\alpha = 0.96$, 0.98, and 0.99, the mean N(t) with two arbitrary sample paths has been shown for $\rho_{\text{ex}} = 0.5\beta$, $\rho_{\text{ex}} = 0.75\beta$, and $\rho_{\text{ex}} = \beta$.

5.3.2 Ramp external reactivity

The numerical solutions of the fractional SNPKE of U^{235} nuclear reactor have been obtained using parameters similar to those in Sect. 5.3.1. Here, the external reactivity is represented as $\rho_{ex} = 0.1t$ and $\rho_{ex} = 0.01t$, the nonlinear coefficient σ takes 10^{-11} or 10^{-13} .

For different ramp external reactivities, i.e., $\rho_{ex} = 0.1t$ and 0.01t, the mean peak values of N(t) with respect to time for fractional orders $\alpha = 0.96$, 0.98, and 0.99 at step size h = 0.001 s and for 500 trials are listed in Table 4a. These results have been compared with the previously



Fig. 6 (Color online) Mean N(t) and two arbitrary sample paths for **a** ramp reactivity $\rho_{\rm ex} = 0.01t$, $\sigma = 10^{-11}$, and $\alpha = 0.96$, **b** ramp reactivity $\rho_{\rm ex} = 0.01t$, $\sigma = 10^{-13}$, and $\alpha = 0.96$, **c** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-11}$, and $\alpha = 0.96$, **c** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-11}$, and $\alpha = 0.96$, **d** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-13}$, and $\alpha = 0.96$





(a) 1010

10⁸

10⁶

104

100

1

1

0

1

Neutron Population



Fig. 7 (Color online) Mean N(t) and two arbitrary sample paths for **a** ramp reactivity $\rho_{\rm ex} = 0.01t$, $\sigma = 10^{-11}$, and $\alpha = 0.98$, **b** ramp reactivity $\rho_{\rm ex} = 0.01t$, $\sigma = 10^{-13}$, and $\alpha = 0.98$, **c** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-11}$, and $\alpha = 0.98$, **d** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-13}$, and $\alpha = 0.98$, **d** ramp reactivity $\rho_{\rm ex} = 0.1t$, $\sigma = 10^{-13}$, and $\alpha = 0.98$

2

Time (s)

3

4

5

 $\alpha = 0.99$



Table 5 Mean peak values of N(t) for sinusoidal reactivity $\rho = 0.005333 \sin(\frac{\pi t}{t})$ for different values of fractional order α

ρ	$\alpha = 0.96$		$\alpha = 0.98$		$\alpha = 0.99$	
	Peak	Time (s)	Peak	Time (s)	Peak	Time (s)
$0.005333\sin\left(\frac{\pi t}{T}\right)$	38.0005	38.28	45.8029	38.18	49.1345	38.99

obtained results [10, 15] in Table 4b with graphical representation in Figs. 6a-c, 7a-c, and 8a-c. The solutions of SPKE obtained using the above-discussed fractional scheme have been tabulated to establish the efficiency of the higher-order approximation method.

5.4 Sinusoidal reactivity

In this section, the reactivity is in the form of sinusoidal change, i.e., $\rho = \rho_0 \sin(\frac{\pi t}{T})$. The numerical solution for this reactivity has been obtained using the following parame- $\rho_0 = 0.005333, \quad \beta_1 = \beta = 0.0079,$ $\lambda_1 = 0.077,$ ters:



Fig. 9 (Color online) Mean N(t) and two arbitrary sample paths for sinusoidal reactivity $\rho = 0.005333 \sin(\frac{\pi t}{T})$ with **a** fractional order $\alpha = 0.96$, **b** fractional order $\alpha = 0.98$, and **c** fractional order $\alpha = 0.99$

 $\Lambda = 0.001$, q = 0, $N(0) = N_0 = 1$, and time period T = 100 s. The mean peak values of N(t) with respect to time for fractional orders $\alpha = 0.96$, 0.98, and 0.99 are presented in Table 5 with graphical representation in Fig. 9.

6 Conclusion

In this study, fractional SPKEs have been solved using the higher-order approximation scheme with different fractional orders α . The obtained numerical solutions for mean N(t) have been presented in the tables and graphically demonstrated to justify the efficiency of the proposed higher-order approximation method. In addition, the results have been compared to some previous works such as [10, 15, 17]. The results obtained by the implemented fractional model are in good agreement with previous results, which further establishes the efficiency of our proposed scheme. The graphical representation for different reactivities shows the behavior of the mean neutron population. The random fluctuations at low power levels and achievement of equilibrium state after reaching its peak value provide us with a succinct idea about the behavior of N(t) for different reactivities.

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