



# Performance of the CENDL-3.2 and other major neutron data libraries for criticality calculations

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**Abstract** Nuclear data are the cornerstones of reactor physics and shielding calculations. Recently, China released CENDL-3.2 in 2020, and the US released ENDF/B-VIII.0 in 2018. Therefore, it is necessary to comprehensively evaluate the criticality computing performance of these newly released evaluated nuclear libraries. In this study, we used the NJOY2016 code to generate ACE format libraries based on the latest neutron data libraries (including CENDL-3.2, JEFF3.3, ENDF/B-VIII.0, and JENDL4.0). The MCNP code was used to conduct a detailed analysis of fission nuclides, including  $^{235}\text{U}$ ,  $^{233}\text{U}$ , and  $^{239}\text{Pu}$ , in different evaluated nuclear data libraries based on 100 benchmarks. The criticality calculation performance of each library was evaluated using three statistical parameters:  $\delta k/\sigma$ ,  $\chi^2$ , and  $\langle|\Delta|\rangle$ . Analysis of the  $\delta k/\sigma$  parameter showed that CENDL-3.1 and JENDL-4.0 both had > 10 benchmarks that exceeded  $3\sigma$ , whereas CENDL-3.2, ENDFB-VIII.0, and JEFF-3.3 had, 7, 5, and 4 benchmarks, respectively, exceeding  $3\sigma$ . The ENDF/B-VII.1 library performed best, with only two benchmarks exceeding  $3\sigma$ . Compared to CENDL-3.1, CENDL-3.2 offers an improvement in criticality calculations. Compared to the JEFF-3.3 and ENDF/B-VIII.0 libraries, CENDL3.2 performs better in the calculation of the  $^{233}\text{U}$  assemblies, but it performs poorly in the pusl11 series case

calculation of the  $^{239}\text{Pu}$  assemblies, and thus further improvement is needed.

**Keywords** Criticality calculations · CENDL-3.2 · ENDF/B-VIII.0 · Neutron · ACE library

## 1 Introduction

Evaluated nuclear data libraries are the basis of reactor physics and shielding calculations. Currently, there are five major evaluated nuclear libraries in the world. Recently, the world's major nuclear data libraries have successively released their latest versions. In 2020, the China Institute of Atomic Energy released CENDL-3.2 [1]. Data for most of the key nuclides in nuclear applications (e.g., U, Pu, Th, and Fe) have been revised and updated in CENDL-3.2. In 2018, the Brookhaven National Laboratory in the US released ENDF/B-VIII.0 [2]. ENDF/B-VIII.0 fully incorporates the new International Atomic Energy Agency standards, includes improved thermal neutron scattering data, and uses newly evaluated data from the CIELO project [3] for neutron reactions on  $^1\text{H}$ ,  $^{16}\text{O}$ ,  $^{56}\text{Fe}$ ,  $^{235}\text{U}$ ,  $^{238}\text{U}$ , and  $^{239}\text{Pu}$ . In 2017, the Nuclear Energy Agency officially released JEFF-3.3 [4], which thoroughly updated the neutron, decay data, fission yields, and neutron activation libraries in EAF format and provided neutron thermal scattering files for 20 compounds. In 2010, the Japan Atomic Energy Agency released JENDL4.0 [5]. In this new library, much emphasis is placed on the improvement of fission products and minor actinoid data. As of 2016, the ENDF files of some nuclides in JENDL4.0 have been updated. In addition, China's nuclear data measurement technology has also progressed, providing effective support

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for the evaluation of the CENDL library. Researchers at the Chinese Academy of Sciences [6] measured the neutron capture cross section of  $^{197}\text{Au}$  using the time-of-flight technique at the Back-n facility of the China Spallation Neutron Source in the 1 eV to 100 keV range. The results are in good agreement with the ENDF/BVIII.0, CENDL-3.1, and other libraries in the resonance region and in agreement with both neutron time-of-flight and GELINA experimental data in the 5–100 keV range. In addition, researchers at Lanzhou University [7] measured cross sections of the (n,2n) reactions for Nd isotopes induced by 14-MeV neutrons using activation and relative methods. The present results are generally consistent with the ENDF/B-VII.1, CENDL-3.1, and JENDL-4.0 data at neutron energies of 14.2 and 14.9 MeV.

An evaluated nuclear data library cannot be used directly and needs to be processed into a working nuclear library using a nuclear data processing code (such as NJOY [8] or NECP-Atlas [9]). In general, working nuclear libraries are divided into multi-group cross-section libraries for deterministic codes and continuous point-wise cross-section libraries for stochastic codes. The ACE format [10] is a common continuous point-wise cross-section library storage format used in stochastic codes for reactor physics and shielding calculations.

From civil nuclear power plants to space reactors for aerospace and power reactors for submarines, many applications have high requirements for nuclear data libraries. Different evaluated nuclear data libraries employ different evaluations for some important reaction channels of key nuclides. Therefore, it is necessary to conduct detailed tests on the quality of nuclear data from different nuclear data libraries. The validation of nuclear data libraries generally includes criticality, shielding, and depletion tests. The criticality benchmark test is an important form of acceptance testing that can effectively test the data accuracy of key fission nuclides and provide effective guidance for thermal and fast reactor designs. In addition, a more detailed understanding of the criticality calculation performance of the newly released evaluated nuclear data libraries is needed to provide a reference for the choice of nuclear data libraries in thermal and fast reactor designs. Hence, it is very important to evaluate the quality of the newly released nuclear library through criticality benchmark testing.

In this study, the MCNP [11] code was used to evaluate the performance of the newly released evaluated nuclear data libraries for criticality calculations. Several criticality benchmarks from the ICSBEP manual [12] were selected to verify the performance of criticality calculations. The criticality calculation performance of each library was evaluated using three statistical parameters:  $\delta k/\sigma$ ,  $\chi^2$ , and

$\langle|\Delta| \rangle$  [13, 14]. The remainder of this paper is organized as follows: Sect. 2 introduces the methods for the development of the ACE libraries, Sect. 3 describes the numerical verification of the newly released libraries, and Sect. 4 presents our conclusions.

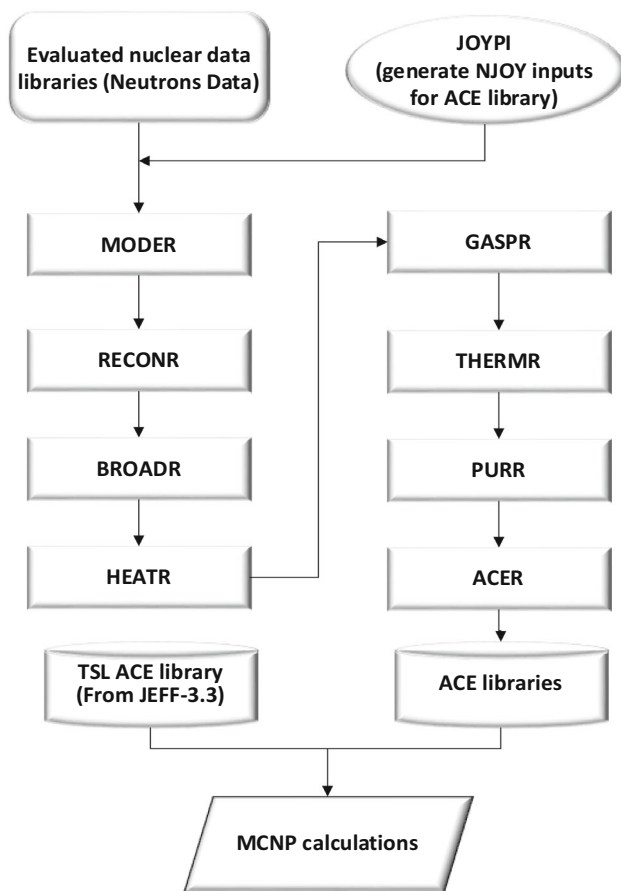
## 2 Methodology

To study the criticality calculation performance of the newly released evaluated nuclear data libraries, the ACE-formatted libraries for Monte Carlo code calculations based on the CENDL-3.1 [15], CENDL-3.2, ENDF/B-VIII.0, ENDF/B-VII.1 [16], JEFF-3.3, and JENDL-4.0 were created using the NJOY2016 code [8]. Based on the criticality benchmarks in the ICSBEP manual, the criticality calculation performance of different evaluated nuclear data libraries was studied in detail using statistical analysis methods. Section 2.1 describes the methods used to develop the ACE-formatted libraries. Section 2.2 describes the ICSBEP benchmark suite. Section 2.3 describes the details of the statistical analysis methods.

### 2.1 ACE-formatted libraries and MCNP simulation details

The ACE library production and MCNP simulation processes are shown in Fig. 1. The NJOY program is a popular nuclear data processing program that can generate nuclear data in multiple formats for shielding and criticality calculations based on the evaluated nuclear data library. The JOYPI code can generate NJOY inputs for the development of the ACE library. The ACE format library is a continuous point section library for Monte Carlo program calculations and can be processed by using the NJOY program. The main NJOY modules used to make the ACE library include RECONR, BROASDR, THERMR, PURR, and ACER. The RECONR module performs the point cross-section resonance reconstruction function based on the ENDF file data. The BROASDR module performs the temperature-related Doppler broadening function. The THERMR module generates the cross sections for free scatters in the thermal energy range. The PURR module calculates the unresolved resonance probability tables, and the ACER module converts the previously generated data into a c-type ACE file for use in MCNP.

In the benchmark suite of the ICSBEP manual, some benchmarks contain thermal neutron scattering materials, and the corresponding thermal neutron scattering sub-library (TSL library) needs to be processed for calculation. For the new versions of ENDF/B-VIII.0, JENDL-4.0, and JEFF-3.3, there are corresponding TSL libraries, but for CENDL-3.2 and CENDL-3.1, no TSL library is provided.



**Fig. 1** Production and verification process for the ACE-formatted libraries. MODER, RECONR, BROADR, HEATR, GASPR, THERMR, PURR, ACER are the modules of the NJOY 2016 code. JOYPI is an automatic NJOY input card generating program

Therefore, to maintain the consistency of verification for different evaluated nuclear data libraries, we used the verified and publicly available data of the ACE thermal scattering library of JEFF-3.3 to perform criticality calculations for the benchmarks with thermal neutron scattering materials. The purpose of this study is to verify the overall criticality calculation performance of neutron data libraries. The standard neutron ACE library used in this study was based on different data libraries and was produced using the NJOY2016 program. If there are moderators in the benchmark facilities, the TSL library must be considered in the calculations. The TSL library used for the benchmark with moderators was from the JEFF3.3 ACE library.

For all assemblies calculated by MCNP, 3000 source neutrons were run per kcode cycle. For all metal assembly benchmarks, 40 inactive cycles and 360 active cycles were run. For the solution assemblies, 40 inactive cycles and 760 active cycles were run. These numbers ensure that sufficient active cycles are run to obtain good statistics for  $k_{\text{eff}}$  calculations [17]. All these benchmarks use the total nuclide

data in the MCNP input. Eigenvalue uncertainties were  $< 70$  pcm, which is approximately an order of magnitude lower than most benchmark uncertainties.

## 2.2 Description for the criticality benchmarks suite

A set of 100 criticality safety benchmarks was selected and established for the MCNP code. Benchmarks were obtained from two reports: a suite of criticality benchmarks for validating nuclear data [17] and an expanded criticality validation suite for MCNP [18]. Among the 100 benchmark cases, 88 were from the first report and 12 were from the second one. Although all benchmark cases have standard ICSBEP names, the names are too long to be displayed in the chart when describing them; therefore, they are usually represented by abbreviations. The abbreviations of the benchmark cases used in this study are consistent with those of the above two reports.

The fission nuclides  $^{233}\text{U}$ ,  $^{235}\text{U}$ , and  $^{239}\text{Pu}$  produce the majority of fission products in the reactor. The criticality benchmark suite in this study is made up of five major categories based on the major fission nuclides: critical assemblies utilizing  $^{233}\text{U}$ , intermediate-enriched  $^{235}\text{U}$  (IEU), highly enriched  $^{235}\text{U}$  (HEU),  $^{239}\text{Pu}$ , and mixed metal (MIX) assemblies. Within each category, there were bare, reflected, and solution assemblies. The classification of the assembly and the number of each classification are listed in Table 1. The ICSBEP benchmarks and their abbreviations and the benchmark  $k_{\text{eff}}$  reference values used in this study are listed in Table 8 in Appendix, and the calculated  $k_{\text{eff}}$  values and statistical errors of each data library are listed in Table 9.

## 2.3 Statistical analysis methods

The benchmark results were analyzed using the statistical parameters  $\delta k/\sigma$ ,  $\chi^2$ , and  $\langle |\Delta| \rangle$ .

$\chi^2$  is a statistical parameter used to determine which evaluated nuclear data library is the most suitable for criticality calculations.  $\langle |\Delta| \rangle$  is the measure of the average difference between the calculated and benchmark  $k_{\text{eff}}$  eigenvalues.  $\delta k/\sigma$  indicates the consistency of the evaluated library and benchmark value in each benchmark case.

We use the  $3\sigma$  rule to evaluate the calculation results of the benchmark. In statistics, the  $3\sigma$  rule is a shorthand used

**Table 1** Start this caption with a short description of your table

| Assembly     | $^{233}\text{U}$ | IEU | HEU | $^{239}\text{Pu}$ | MIX | Total |
|--------------|------------------|-----|-----|-------------------|-----|-------|
| Case numbers | 17               | 14  | 37  | 21                | 11  | 100   |

to remember the percentage of values that lie within an interval estimate in a normal distribution: 68%, 95%, and 99.7% of the values lie within one, two, and three standard deviations of the mean, respectively. In empirical sciences, the  $3\sigma$  rule expresses a conventional heuristic that nearly all values are taken to lie within three standard deviations of the mean, and thus it is empirically useful to treat 99.7% probability as near certainty. The results can be considered identical if the relative difference between the  $k_{\text{eff}}$  eigenvalues and the benchmark values was within the  $\pm 3\sigma$  interval. Note that we have bolded the values exceeding  $\pm 3\sigma$  in each benchmark to facilitate identification in the table.

$\langle|\Delta|\rangle$  and  $\chi^2$  are defined by

$$\langle|\Delta|\rangle = \sum_{i=1}^n \frac{|k_{\text{eff}_i}^{\text{calculation}} - k_{\text{eff}_i}^{\text{benchmark}}|}{n}, \quad (1)$$

$$\chi^2 = \sum_{i=1}^n \frac{((k_{\text{eff}_i}^{\text{calculation}} - k_{\text{eff}_i}^{\text{benchmark}})/\sigma_i^{\text{benchmark}})^2}{n}, \quad (2)$$

where  $n$  is the benchmark number,  $\sigma^{\text{benchmark}}$  is the benchmark experimental uncertainty,  $k_{\text{eff}}^{\text{calculation}}$  and  $k_{\text{eff}}^{\text{benchmark}}$  are the simulated  $k_{\text{eff}}$  eigenvalue and benchmark  $k_{\text{eff}}$  eigenvalue, respectively, and  $i$  and  $n$  are the specific benchmark and total number of benchmark cases, respectively.  $\delta k/\sigma$  was used to provide a confidence level for the benchmarks. The relative difference  $\delta k$  and the relative combined statistical uncertainty  $\sigma$  are defined by

$$\delta k = \frac{k_{\text{eff}}^{\text{calculation}} - k_{\text{eff}}^{\text{benchmark}}}{k_{\text{eff}}^{\text{benchmark}}}, \quad (3)$$

$$\sigma = \sqrt{(\sigma^{\text{benchmark}} \cdot k_{\text{eff}}^{\text{benchmark}})^2 + (\sigma^{\text{calculation}} \cdot k_{\text{eff}}^{\text{calculation}})^2}. \quad (4)$$

$\chi^2$  and  $\langle|\Delta|\rangle$  are lumped parameters that can describe the overall performance of the data library in the corresponding types of benchmarks.  $\delta k/\sigma$  can locate the performance of each data library in each benchmark.

### 3 Results and discussion

#### 3.1 Comparison of the $k_{\text{eff}}$ calculation results

The calculated values were compared to the reference value (Figs. 2, 3, 4, 5, 6). Most of the calculated values were close to the allowable error interval of the experimental value. The analysis and discussion of each benchmark type are as follows:

- (1) For the  $^{233}\text{U}$  assemblies (Fig. 2), the calculated values in most cases were in good agreement with

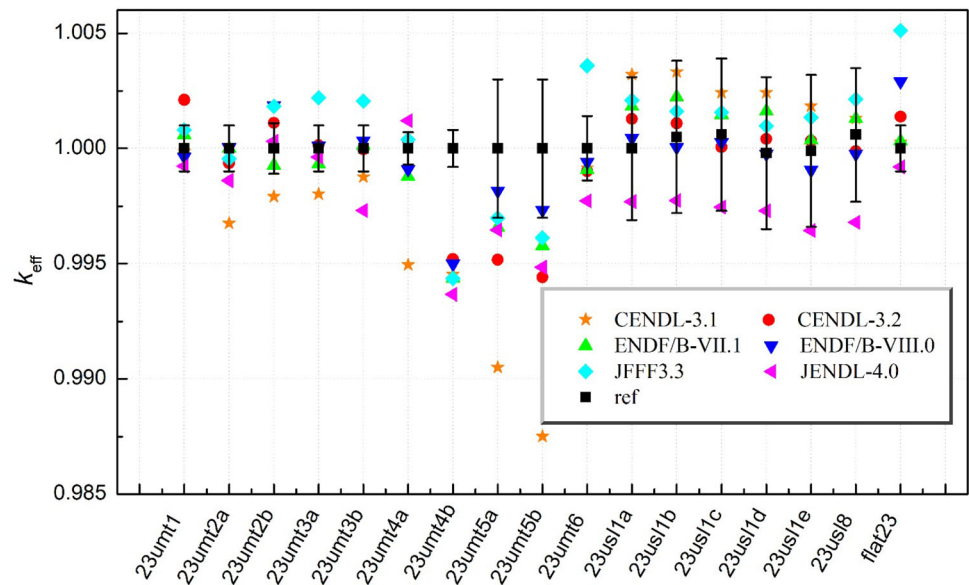
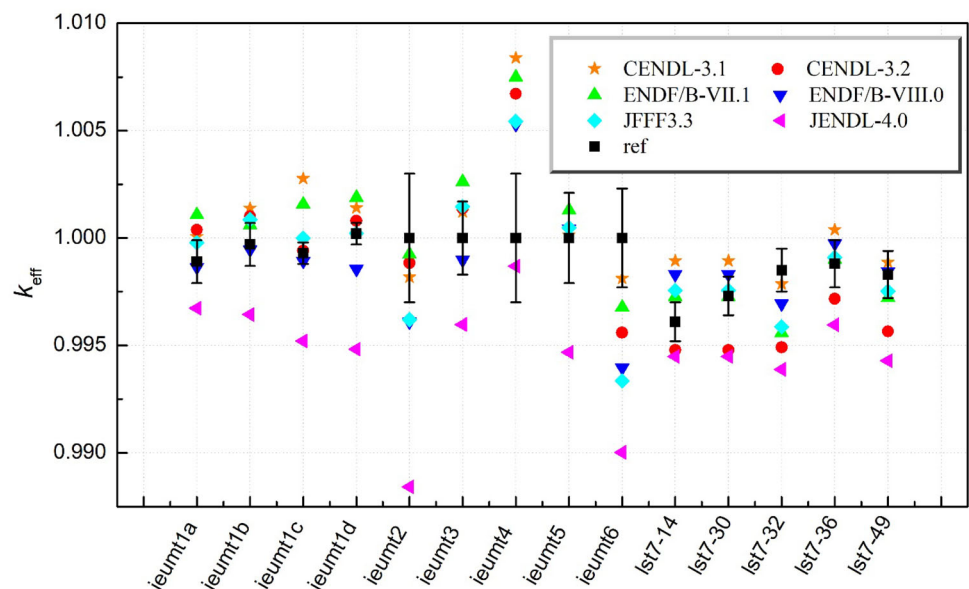
the experimental values. The calculated values of the benchmarks of 23umt4b deviated significantly from the experimental values.

- (2) For the IEU assemblies (Fig. 3), the calculated values in most cases were in good agreement with the experimental values. For the ieuimt4 benchmark, all the calculated results except JENDL-4.0 were overestimated compared to the experimental value, and, for the ieuimt6 benchmark, all the calculated results were underestimated compared to the experimental value.
- (3) For the HEU assemblies (Fig. 4), all calculated values were overestimated compared to the experimental values in the umet3k benchmark. For the umet9b, usol13c, umet8, and umet15 benchmarks, all calculated values were underestimated compared to the experimental values.
- (4) For the  $^{239}\text{Pu}$  assemblies (Fig. 5), the calculated values in most cases were in good agreement with the experimental values. For the four benchmarks of the pusl cases (pusl11a, pusl11b, pusl11c, and pusl11d), the calculation results of CENDL-3.2 and CENDL-3.1 were overestimated compared to those of other data libraries. After comparing individual nuclides to each other, we found that  $^{239}\text{Pu}$  of CENDL-3.2 caused the overestimation of pusl11 series cases.
- (5) For the MIX assemblies (Fig. 6), the calculated values in most cases were in good agreement with the experimental values. The calculated values of mix-met8-7 deviate greatly from the experimental values.

#### 3.2 Discussion of the statistical results

The results of the three statistical parameters of each data library (Tables 2, 3, 4, 5, 6) were compared in this study. The analysis and discussion are as follows:

- (1) For the  $^{233}\text{U}$  assemblies (Table 2), CENDL-3.1 exceeded  $3\sigma$  in the four benchmarks of 23umt4a, 23umt4b, 23umt5a, and 23umt5b. JEFF-3.3 exceeded  $3\sigma$  in the flat23 benchmark. For the 23umt4b benchmark, all databases exceeded  $3\sigma$ . By analyzing the values of  $\chi^2$  and  $\langle|\Delta|\rangle$ , it can be concluded that CENDL-3.2 offers significant improvement compared to CENDL-3.1.
- (2) For the IEU assemblies (Table 3), CENDL-3.1 exceeded  $3\sigma$  in the benchmarks of 1st7-14 and ieuimt1c. Six benchmarks exceeded  $3\sigma$  in the JENDL-4.0 library. Analysis of the values of  $\chi^2$  and  $\langle|\Delta|\rangle$  showed that ENDFB-VIII.0 and JEFF-3.3 performed better than the other libraries.
- (3) For the HEU assemblies (Table 4), CENDL-3.1 exceeded  $3\sigma$  in the benchmarks of umet19 and

**Fig. 2** (Color online)  $k_{\text{eff}}$  comparison for  $^{233}\text{U}$  assemblies**Fig. 3** (Color online)  $k_{\text{eff}}$  comparison for IEU assemblies

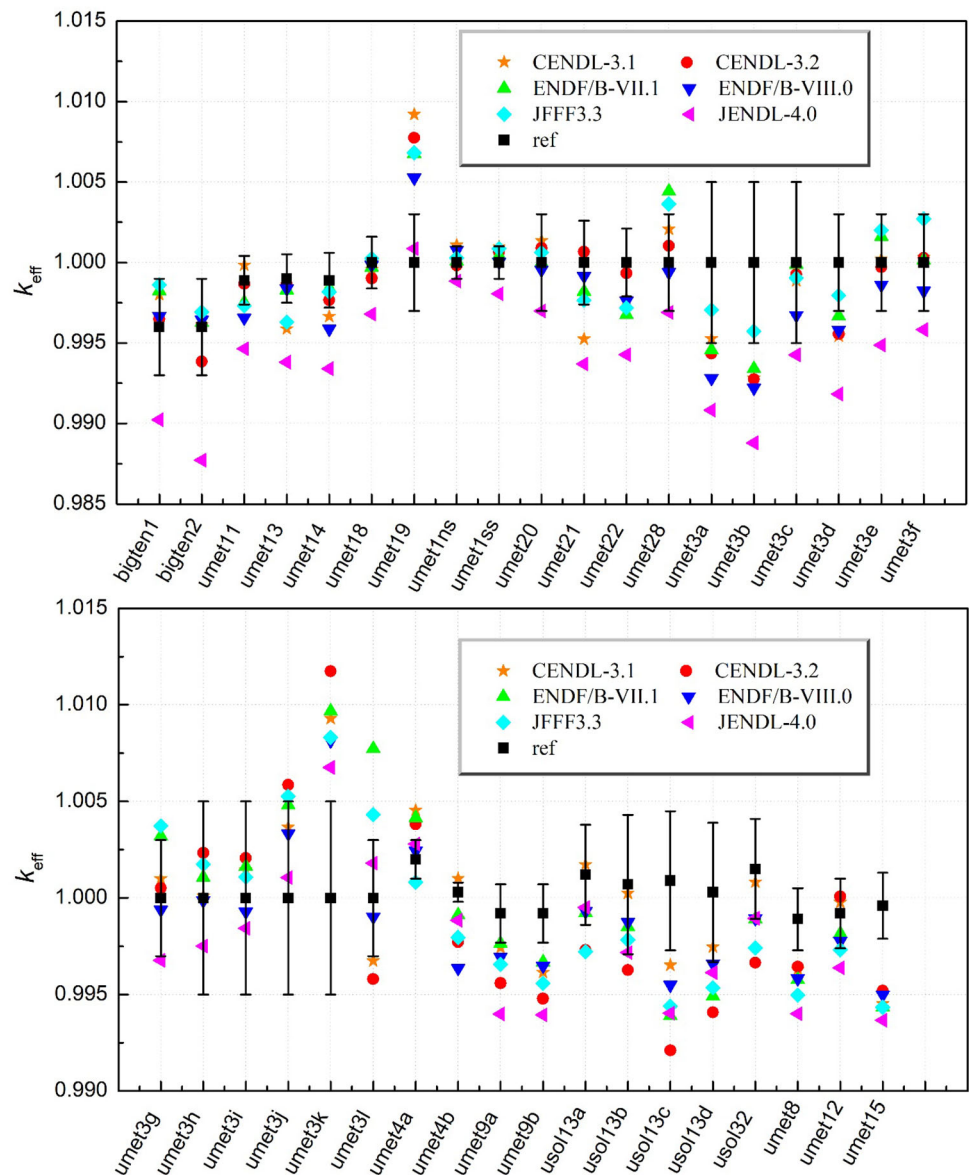
ieumt1c. JEFF-3.3 exceeded  $3\sigma$  in the umet4b benchmark. Five benchmarks exceeded  $3\sigma$  in the JENDL-4.0 library. Analysis of the values of  $\chi^2$  and  $\langle|\Delta| \rangle$  showed that CENDL-3.2 is not significantly improved compared to CENDL-3.1.

- (4) For the  $^{239}\text{Pu}$  assemblies (Table 5), CENDL-3.1, and CENDL-3.2 both exceeded  $3\sigma$  in the benchmarks of pusl11c and pusl11d. For the pumet8b benchmark, except for ENDF/B-VII.1, all other data libraries exceeded  $3\sigma$ . Analyzing the values of  $\chi^2$  and  $\langle|\Delta| \rangle$  showed that the ENDF/B-VII.1 library performs better than the other data libraries.

- (5) For the MIX assemblies (Table 6), all libraries exceeded  $3\sigma$  in the benchmark mixmet8-7. The ENDF/B-VII.1 library performs better than the other data libraries. Analysis of the values of  $\chi^2$  and  $\langle|\Delta| \rangle$  shows that CENDL-3.2 performs better than CENDL-3.1.

Based on the calculated values of all benchmarks, we used chi-square and average errors to analyze the overall performance of all data libraries in criticality calculations (Table 7). From the perspective of the calculation results of the new and old updates of the library, CENDL-3.2 has smaller chi-square and average deviations for all

**Fig. 4** (Color online)  $k_{\text{eff}}$  comparison for HEU assemblies

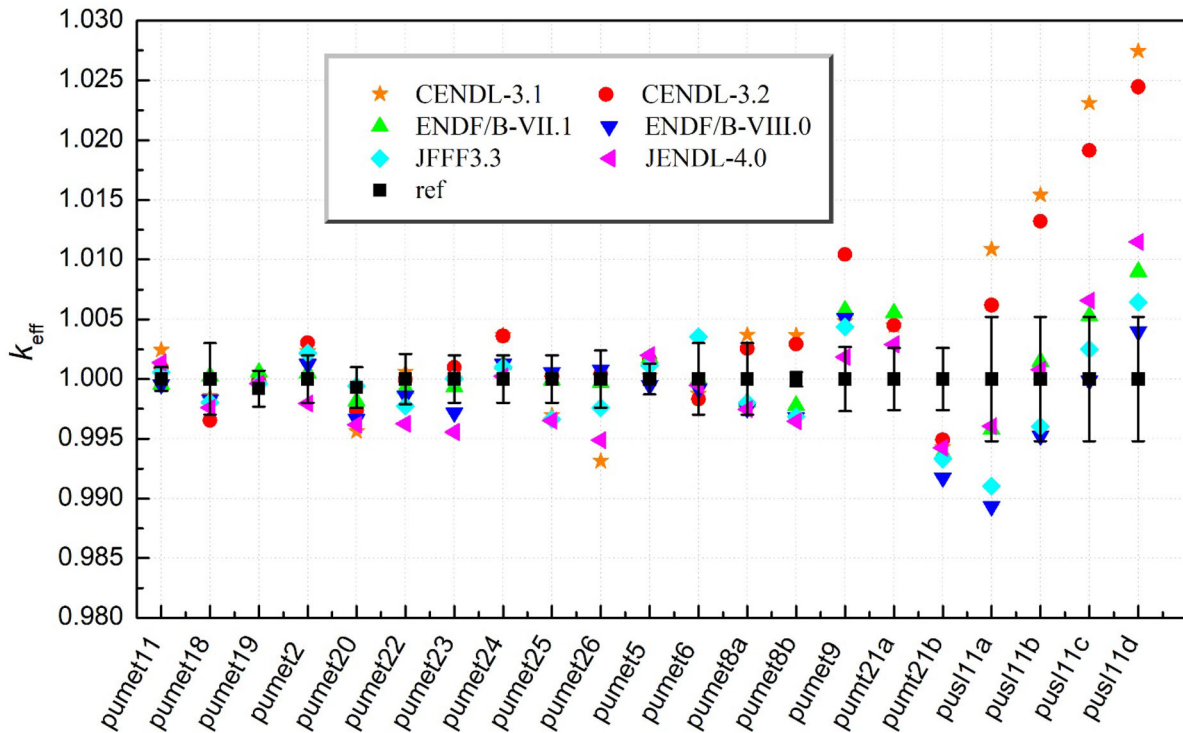


benchmarks than CENDL-3.1, which reflects that, for the type of benchmarks involved, CENDL-3.2 is superior to the previous version. The average deviation of ENDF/B-VIII.0 for all benchmarks is similar to that of ENDF/B-VII.1, both being near 230, and the chi-square is larger than that of ENDF/B-VII.1. By counting the number of benchmarks exceeding  $3\sigma$ , it can be seen that the number of benchmarks exceeding  $3\sigma$  for JENDL-4.0 and CENDL-3.1 is  $> 10$  and the number of benchmarks exceeding  $3\sigma$  for ENDF/B-VIII.0 and JEFF-3.3 is  $\sim 5$ .

In general, based on the above 100 criticality benchmark calculation results, we can conclude that the criticality calculation performance of CENDL-3.2 is better than that of CENDL-3.1. Analysis of the chi-square and average deviations and the number of benchmarks exceeding  $3\sigma$

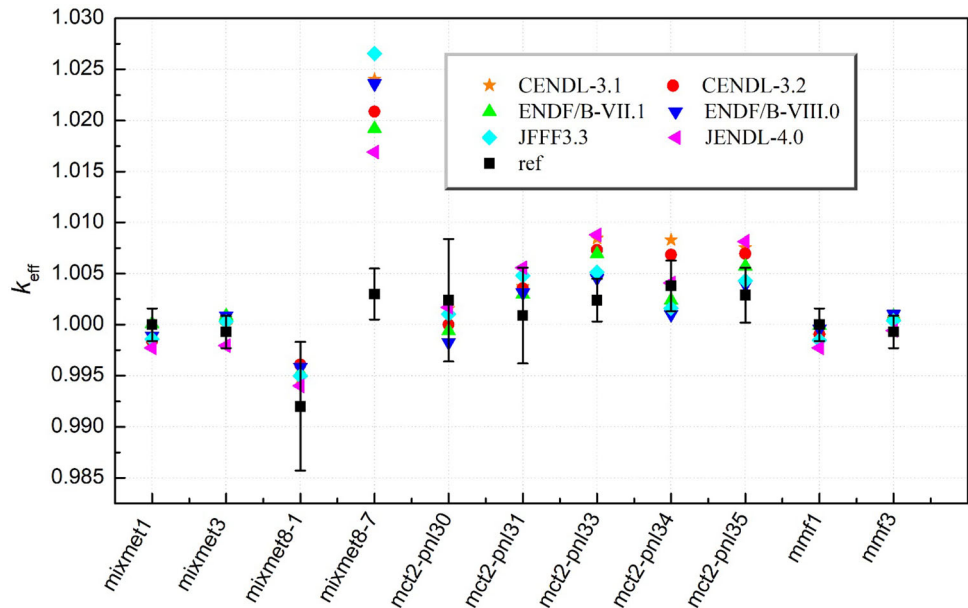
demonstrates that the overall criticality calculation performance of ENDF/B-VIII.0 and JEFF3.3 is equivalent. The ENDF/B-VII.1 library performed the best. Compared with the JEFF-3.3 and ENDF/B-VIII.0 libraries, CENDL3.2 performs better in the calculation of  $^{233}\text{U}$  devices and performs poorly in the pusl11 series case calculation of Pu devices, and thus further improvement is needed.

Compared to CENDL-3.1, CENDL-3.2 [1] has more materials (272), of which the data of 134 nuclides are new or updated evaluations in the energy region of  $10^{-5}$  eV to 20 MeV. Data for most of the key nuclides in nuclear applications (e.g., U, Pu, Th, and Fe) have been revised. Covariance data for the main reactions were added for 70 fission product nuclides in CENDL-3.2. Compared to



**Fig. 5** (Color online)  $k_{\text{eff}}$  comparison for  $^{239}\text{Pu}$  assemblies

**Fig. 6** (Color online)  $k_{\text{eff}}$  comparison for MIX assemblies



ENDF/B-VII.1, ENDF/B-VIII.0 [2] employs major changes for neutron reactions on the important isotopes  $^1\text{H}$ ,  $^{16}\text{O}$ ,  $^{56}\text{Fe}$ ,  $^{235}\text{U}$ ,  $^{238}\text{U}$ , and  $^{239}\text{Pu}$  and other nuclides that impact simulations of nuclear criticality. The number of materials increased from 423 to 557. In addition, neutron reactions on light nuclei, structural materials, minor actinides, fission energy release, decay data, and charged particle reactions

and thermal neutron scattering data have been notably updated.

Therefore, we expect that the criticality calculation performance of ENDF/B-VIII.0 is better than that of ENDF/B-VII.1. However, for different benchmark experiments, the calculation results of the new evaluated library ENDF/B-VIII.0 are not all better than those of the previous

**Table 2** The statistic metrics for  $^{233}\text{U}$  assemblies

| Case                     | CENDL-3.1<br>$\delta k/\sigma$ | CENDL-3.2     | ENDF/B-VII.1  | ENDF/B-VIII.0 | JEFF-3.3      | JENDL-4.0     |
|--------------------------|--------------------------------|---------------|---------------|---------------|---------------|---------------|
| 23umt1                   | − 0.11                         | 1.82          | 0.52          | −0.33         | 0.70          | −0.67         |
| 23umt2a                  | − 2.84                         | − 0.55        | 0.00          | 0.03          | − 0.39        | − 1.22        |
| 23umt2b                  | − 1.69                         | 0.90          | − 0.58        | 1.50          | 1.45          | 0.25          |
| 23umt3a                  | − 1.70                         | 0.12          | − 0.58        | 0.10          | 1.89          | − 0.33        |
| 23umt3b                  | − 1.05                         | − 0.03        | 0.12          | 0.28          | 1.77          | − 2.28        |
| 23umt4a                  | − <b>5.57</b>                  | 0.37          | − 1.33        | − 1.03        | 0.41          | 1.28          |
| 23umt4b                  | − <b>5.64</b>                  | − <b>4.84</b> | − <b>5.75</b> | − <b>5.26</b> | − <b>5.76</b> | − <b>6.38</b> |
| 23umt5a                  | − <b>3.10</b>                  | − 1.58        | − 1.11        | − 0.60        | − 0.99        | − 1.15        |
| 23umt5b                  | − 4.07                         | − 1.82        | − 1.38        | − 0.87        | − 1.26        | − 1.68        |
| 23umt6                   | − 0.55                         | − 0.63        | − 0.62        | − 0.39        | 2.31          | − 1.46        |
| 23usl1a                  | 1.03                           | 0.41          | 0.59          | 0.14          | 0.67          | − 0.74        |
| 23usl1b                  | 0.85                           | 0.18          | 0.52          | − 0.14        | 0.34          | − 0.83        |
| 23usl1c                  | 0.55                           | − 0.16        | 0.26          | − 0.10        | 0.29          | − 0.94        |
| 23usl1d                  | 0.79                           | 0.18          | 0.55          | − 0.01        | 0.35          | − 0.75        |
| 23usl1e                  | 0.59                           | 0.13          | 0.14          | − 0.25        | 0.44          | − 1.04        |
| 23usl8                   | 0.24                           | − 0.25        | 0.24          | − 0.29        | 0.53          | − 1.30        |
| flat23                   | 0.23                           | 1.16          | 0.27          | 2.44          | <b>4.25</b>   | − 0.67        |
| $\chi^2$                 | 14.88                          | 1.65          | 2.71          | 3.29          | 3.22          | 1.85          |
| $\langle \Delta \rangle$ | 351.8                          | 142.5         | 144.3         | 115.9         | 196.9         | 225.4         |

The values in bold indicate that the values of  $\delta k/\sigma$  have exceeded  $\pm 3$ , indicating that the calculated result of this benchmark are in poor consistency with the experimental value

**Table 3** The statistic metrics for IEU assemblies

| Case                     | CENDL-3.1<br>$\delta k/\sigma$ | CENDL-3.2     | ENDF/B-VII.1 | ENDF/B-VIII.0 | JEFF-3.3 | JENDL-4.0     |
|--------------------------|--------------------------------|---------------|--------------|---------------|----------|---------------|
| 1st7-14                  | <b>3.02</b>                    | − 1.39        | 1.24         | 2.34          | 1.56     | − 1.70        |
| 1st7-30                  | 1.74                           | − 2.65        | − 0.04       | 1.07          | 0.28     | − 2.97        |
| 1st7-32                  | − 0.61                         | − <b>3.45</b> | − 2.80       | − 1.50        | − 2.55   | − <b>4.42</b> |
| 1st7-36                  | 1.41                           | − 1.44        | 0.18         | 0.84          | 0.27     | − 2.51        |
| 1st7-49                  | 0.50                           | − 2.33        | − 0.97       | 0.12          | − 0.69   | − <b>3.56</b> |
| ieumt1a                  | 1.00                           | 1.27          | 1.91         | − 0.23        | 0.76     | − 1.88        |
| ieumt1b                  | 1.45                           | 1.13          | 0.79         | − 0.21        | 1.00     | − 2.80        |
| ieumt1c                  | <b>4.40</b>                    | 0.14          | 2.92         | − 0.48        | 0.92     | − <b>5.26</b> |
| ieumt1d                  | 1.53                           | 0.79          | 2.19         | − 2.04        | 0.03     | − <b>7.03</b> |
| ieumt2                   | −0.60                          | − 0.38        | − 0.25       | − 1.28        | − 1.25   | − <b>3.79</b> |
| ieumt3                   | 0.68                           | 0.77          | 1.44         | − 0.56        | 0.82     | − 2.23        |
| ieumt4                   | 2.74                           | 2.20          | 2.45         | 1.73          | 1.77     | − 0.43        |
| ieumt5                   | 0.07                           | 2.13          | 0.60         | 0.20          | 0.22     | − 2.45        |
| ieumt6                   | − 0.79                         | − 1.86        | − 1.36       | − 2.55        | − 2.80   | − <b>4.21</b> |
| $\chi^2$                 | 5.98                           | 3.61          | 4.28         | 2.43          | 2.02     | 21.26         |
| $\langle \Delta \rangle$ | 202.1                          | 239.5         | 198.9        | 179.0         | 185.9    | 449.7         |

The values in bold indicate that the values of  $\delta k/\sigma$  have exceeded  $\pm 3$ , indicating that the calculated result of this benchmark are in poor consistency with the experimental value

version, such as the three benchmarks of pusl11a, pusl11b, and pumet21b in the Pu assemblies. In the criticality calculation of these three benchmarks, compared with the experimental value, the  $k_{\text{eff}}$  results of ENDF/B-VIII.0 are

200–500 pcm smaller than the calculation results of ENDF/B-VII.1. This is also one of the goals of our work, that is, to find benchmarks that are not sensitive to the newly evaluated library and provide a reference for subsequent

**Table 4** The statistic metrics for HEU assemblies

| Case                     | CENDL-3.1<br>$\delta k/\sigma$ | CENDL-3.2 | ENDF/B-VII.1 | ENDF/B-VIII.0 | JEFF-3.3 | JENDL-4.0     |
|--------------------------|--------------------------------|-----------|--------------|---------------|----------|---------------|
| umet11                   | 0.57                           | − 0.13    | − 0.83       | − 1.41        | − 0.95   | − 2.53        |
| bigten1                  | 0.67                           | 0.16      | 0.74         | 0.22          | 0.87     | − 1.92        |
| bigten2                  | 0.04                           | − 0.71    | 0.09         | 0.15          | 0.31     | − 2.75        |
| umet13                   | − 1.93                         | − 0.22    | − 0.44       | − 0.38        | − 1.68   | − <b>3.22</b> |
| umet14                   | − 1.25                         | − 0.68    | − 0.27       | − 1.67        | − 0.40   | − <b>3.06</b> |
| umet18                   | − 0.25                         | − 0.57    | − 0.17       | − 0.09        | 0.15     | − 1.89        |
| umet19                   | <b>3.01</b>                    | 2.53      | 2.20         | 1.72          | 2.23     | 0.28          |
| umet1ns                  | 0.93                           | −0.15     | 0.08         | 0.65          | 0.24     | − 0.99        |
| umet1ss                  | 0.85                           | 0.56      | 0.37         | 0.03          | 0.74     | − 1.70        |
| umet20                   | 0.44                           | 0.29      | 0.00         | − 0.15        | 0.20     | − 0.98        |
| umet21                   | − 1.78                         | 0.25      | − 0.67       | − 0.31        | − 0.88   | − 2.37        |
| umet22                   | − 1.02                         | − 0.30    | − 1.48       | − 1.09        | − 1.29   | − 2.63        |
| umet28                   | 0.68                           | 0.34      | 1.45         | − 0.20        | 1.19     | − 1.01        |
| umet3a                   | − 0.94                         | − 1.12    | − 1.08       | − 1.43        | − 0.58   | − 1.82        |
| umet3b                   | − 1.43                         | − 1.44    | − 1.31       | − 1.55        | − 0.85   | − 2.22        |
| umet3c                   | − 0.22                         | − 0.14    | − 0.02       | − 0.65        | − 0.19   | − 1.14        |
| umet3d                   | − 1.49                         | − 1.45    | − 1.08       | − 1.37        | − 0.66   | − 2.67        |
| umet3e                   | 0.07                           | − 0.09    | 0.52         | − 0.45        | 0.65     | − 1.67        |
| umet3f                   | 0.10                           | 0.09      | 0.05         | − 0.57        | 0.88     | − 1.36        |
| umet3g                   | 0.32                           | 0.17      | 1.05         | − 0.20        | 1.22     | − 1.05        |
| umet3h                   | 0.02                           | 0.46      | 0.21         | − 0.03        | 0.35     | − 0.49        |
| umet3i                   | 0.29                           | 0.41      | 0.32         | − 0.14        | 0.21     | − 0.31        |
| umet3j                   | 0.73                           | 1.16      | 0.96         | 0.66          | 1.05     | 0.21          |
| umet3k                   | 1.84                           | 2.33      | 1.92         | 1.62          | 1.65     | 1.34          |
| umet3l                   | − 1.06                         | − 1.37    | 2.51         | − 0.32        | 1.41     | 0.59          |
| umet4a                   | 2.07                           | 1.46      | 1.74         | 0.34          | − 0.97   | 0.64          |
| umet4b                   | 0.81                           | − 2.96    | − 1.36       | − <b>4.29</b> | − 2.62   | − 1.68        |
| umet9a                   | − 1.09                         | − 2.22    | − 0.96       | − 1.40        | − 1.60   | − <b>3.23</b> |
| umet9b                   | − 1.88                         | − 2.72    | − 1.54       | − 1.67        | − 2.25   | − <b>3.26</b> |
| usol13a                  | 0.20                           | − 1.48    | − 0.75       | − 0.72        | − 1.51   | − 0.64        |
| usol13b                  | − 0.13                         | − 1.22    | − 0.61       | − 0.54        | − 0.79   | − 0.97        |
| usol13c                  | − 1.20                         | − 2.42    | − 1.93       | − 1.49        | − 1.79   | − 1.89        |
| usol13d                  | − 0.78                         | − 1.71    | − 1.48       | − 1.02        | − 1.36   | − 1.15        |
| usol32                   | − 0.26                         | − 1.85    | − 0.99       | − 0.98        | − 1.56   | − 0.98        |
| umet8                    | − 1.53                         | − 1.43    | − 1.84       | − 1.81        | − 2.31   | − 2.90        |
| umet12                   | 0.30                           | 0.46      | − 0.56       | − 0.75        | − 0.98   | − 1.49        |
| umet15                   | − 2.84                         | − 2.45    | − 2.93       | − 2.60        | − 2.93   | − <b>3.30</b> |
| $\chi^2$                 | 1.68                           | 2.53      | 1.75         | 2.86          | 2.31     | 4.23          |
| $\langle \Delta \rangle$ | 250.1                          | 299.5     | 279.5        | 245.9         | 293.8    | 432           |

The values in bold indicate that the values of  $\delta k/\sigma$  have exceeded  $\pm 3$ , indicating that the calculated result of this benchmark are in poor consistency with the experimental value

evaluation work. The calculation results of Table 7 list only the statistical performance of the current benchmark cases. The results in Table 7 cannot explain that the calculation result of ENDF/B-VIII.0 must be better than the calculation result of ENDF/B-VII.1. This requires a specific analysis based on specific issues.

### 3.3 Discussion of the anomalous benchmarks

From the discussion in Sect. 3.2, the  $\delta k/\sigma$  value of all data libraries exceeded  $3\sigma$  in the three benchmarks of 23umt4b, pumet8b, and mixmet8-7, which indicates that there is a large deviation between the experimental and

**Table 5** The statistic metrics for  $^{239}\text{Pu}$  assemblies

| Case                       | CENDL-3.1<br>$\delta k/\sigma$ | CENDL-3.2   | ENDF/B-VII.1 | ENDF/B-VIII.0 | JEFF-3.3      | JENDL-4.0     |
|----------------------------|--------------------------------|-------------|--------------|---------------|---------------|---------------|
| pumet1                     | 1.22                           | 1.05        | 0.15         | 0.04          | − 0.23        | − 0.58        |
| pumet10                    | − 0.78                         | − 0.80      | − 0.18       | − 1.07        | 0.01          | − 1.96        |
| pumet11                    | 1.90                           | 0.76        | − 0.38       | − 0.37        | 0.45          | 1.12          |
| pumet18                    | − 0.48                         | − 1.14      | 0.08         | − 0.56        | − 0.64        | − 0.78        |
| pumet2                     | 1.12                           | 1.46        | 0.24         | 0.61          | 1.04          | − 0.99        |
| pumet20                    | − 2.04                         | − 1.06      | − 0.64       | − 1.48        | 0.07          | − 1.74        |
| pumet22                    | 0.28                           | − 0.02      | − 0.35       | − 0.65        | − 1.05        | − 1.73        |
| pumet23                    | 0.00                           | 0.47        | − 0.31       | − 1.36        | 0.01          | − 2.12        |
| pumet24                    | 1.75                           | 1.72        | 0.59         | 0.61          | 0.48          | 0.11          |
| pumet25                    | − 1.46                         | 0.11        | − 0.04       | 0.27          | − 1.62        | − 1.67        |
| pumet26                    | − 2.79                         | 0.17        | − 0.13       | 0.31          | − 0.97        | − 2.07        |
| pumet5                     | 0.17                           | 1.15        | 1.22         | − 0.36        | 0.78          | 1.39          |
| pumet6                     | − 0.40                         | − 0.55      | − 0.01       | − 0.27        | 1.15          | − 0.17        |
| pumet8a                    | 1.21                           | 0.83        | − 0.63       | − 0.81        | − 0.65        | − 0.83        |
| pumet8b                    | <b>4.25</b>                    | <b>3.41</b> | − 2.55       | − <b>4.01</b> | − <b>3.74</b> | − <b>4.13</b> |
| pumet9                     | 1.75                           | <b>3.76</b> | 2.08         | 1.84          | 1.58          | 0.66          |
| pumt21b                    | − 2.14                         | − 1.91      | − 2.35       | − <b>3.08</b> | − 2.50        | − 2.16        |
| pusl11a                    | 2.08                           | 1.18        | − 0.81       | − 2.04        | − 1.72        | − 0.76        |
| pusl11b                    | 2.95                           | 2.53        | 0.28         | − 0.91        | − 0.76        | 0.15          |
| pusl11c                    | <b>4.41</b>                    | <b>3.65</b> | 1.01         | − 0.02        | 0.48          | 1.26          |
| pusl11d                    | <b>5.24</b>                    | <b>4.67</b> | 2.98         | 0.59          | 1.54          | 2.19          |
| $\chi^2$                   | 6.50                           | 4.75        | 1.55         | 2.71          | 2.49          | 3.72          |
| $\langle  \Delta  \rangle$ | 592.3                          | 503.2       | 209.6        | 261.9         | 272.2         | 333.3         |

The values in bold indicate that the values of  $\delta k/\sigma$  have exceeded  $\pm 3$ , indicating that the calculated result of this benchmark are in poor consistency with the experimental value

**Table 6** The statistic metrics for MIX assemblies

| Case                       | CENDL-3.1<br>$\delta k/\sigma$ | CENDL-3.2   | ENDF/B-VII.1 | ENDF/B-VIII.0 | JEFF-3.3    | JENDL-4.0   |
|----------------------------|--------------------------------|-------------|--------------|---------------|-------------|-------------|
| mct2-pnl30                 | − 0.14                         | − 0.40      | − 0.50       | − 0.69        | − 0.23      | − 0.12      |
| mixmet1                    | − 0.56                         | − 0.94      | 0.05         | − 0.64        | − 0.84      | − 1.33      |
| mixmet3                    | 0.35                           | 0.84        | 0.89         | 0.91          | 0.58        | − 0.79      |
| mixmet8-1                  | 0.45                           | 0.65        | 0.52         | 0.62          | 0.48        | 0.32        |
| mixmet8-7                  | <b>8.33</b>                    | <b>7.09</b> | <b>6.42</b>  | <b>8.17</b>   | <b>9.33</b> | <b>5.52</b> |
| mct2-pnl31                 | 0.59                           | 0.56        | 0.43         | 0.47          | 0.82        | 0.98        |
| mct2-pnl33                 | 2.83                           | 2.31        | 2.12         | 1.01          | 1.28        | 2.98        |
| mct2-pnl34                 | 1.78                           | 1.21        | − 0.55       | − 1.10        | − 0.86      | 0.11        |
| mct2-pnl35                 | 1.70                           | 1.49        | 1.03         | 0.38          | 0.52        | 1.92        |
| mmf1                       | − 0.69                         | − 0.59      | − 0.04       | − 0.24        | − 0.94      | − 1.40      |
| mmf3                       | 0.78                           | 0.85        | 0.94         | 1.07          | 0.67        | 0.08        |
| $\chi^2$                   | 7.94                           | 5.83        | 4.60         | 6.74          | 8.62        | 4.53        |
| $\langle  \Delta  \rangle$ | 423.6                          | 404.0       | 332.1        | 378.5         | 392.4       | 356.7       |

The values in bold indicate that the values of  $\delta k/\sigma$  have exceeded  $\pm 3$ , indicating that the calculated result of this benchmark are in poor consistency with the experimental value

calculated values. This question needs to be addressed separately.

The 23umt4b (u233-fast-met-004) benchmark is a spherical device, divided into two layers: The inner layer contains  $^{233}\text{U}$  fuel and the outer layer is a reflective layer

**Table 7** The comparison of  $\langle|\Delta|\rangle$  values (in pcm) and  $\chi^2$  for total benchmark cases

| Metrics                  | CENDL-3.2 | CENDL-3.1 | ENDF/B-VIII.0 | ENDF/B-VII.1 | JEFF-3.3 | JENDL-4.0 |
|--------------------------|-----------|-----------|---------------|--------------|----------|-----------|
| $\chi^2$                 | 3.59      | 5.19      | 3.25          | 2.67         | 3.61     | 6.71      |
| $\langle \Delta \rangle$ | 320.6     | 347.3     | 232.3         | 237.12       | 272.4    | 374.8     |
| Numbers exceed $3\sigma$ | 7         | 11        | 5             | 2            | 4        | 13        |

dominated by tungsten. The pumet8b (pu-met-fast-008b) benchmark is a spherical device, divided into two layers: The inner layer contains Pu fuel and the outer layer is a reflection layer of  $^{232}\text{Th}$ . The mixmet8-7 (mix-met-inter-008-case-7) benchmark is based on a  $k_\infty$  measurement. The configuration consists of a rectangular plate with three rectangular normal-uranium plates above it and the other three below it. The plates were enclosed on all sides of a rectangular steel sheath.

Physically,  $k_{\text{eff}}$  is mainly dominated by fission nuclides, but the reflective layer also has an important influence on  $k_{\text{eff}}$ . The average deviation between the pumet8b and 23umt4b benchmarks and the experimental values was  $\sim 600$  pcm. In fact, there are benchmarks that have a deviation of  $> 600$  pcm from the experimental value, such as the JEFF-3.3 calculation result for pumt21b. For the mixmet8-7 benchmark, the  $k_{\text{eff}}$  deviation between the calculated value of all libraries and the experimental value was within 1000–2000 pcm. In addition, the  $k_{\text{eff}}$  results of the reference values from ENDF/B-VII.0 and ENDF/B-VI also deviate from the experimental values by  $> 1000$  pcm. The  $k_{\text{eff}}$  result of MCNP6.2 based on ENDF/B-VII.1, found in the LA-UR-17-25,040 report [19], is 1.0192, which has a deviation of 1620 pcm from the experimental value. At present, no report has been published to explain the reason for the large deviation between the calculated and experimental values for mixmet8-7, and further research is needed.

From the point of view of nuclear data, because the benchmark involves many nuclides, it is impossible to determine which nuclides that have a greater impact on  $k_{\text{eff}}$  through qualitative analysis. The commonly used method is to determine the important reaction channels of key nuclides that have a greater impact on  $k_{\text{eff}}$  through sensitivity and uncertainty analyses. This part of the work has not been done yet, and the sensitivity and uncertainty analysis will be further studied in our future work.

## 4 Conclusion

A comprehensive suite of 100 criticality benchmarks has been established for validating nuclear data, including CENDL-3.2, ENDF/B-VIII.0, JEFF3.3, JENDL-4.0, CENDL-3.1, and ENDF/B-VII.1. The suite contains benchmarks for five major categories: critical assemblies utilizing  $^{233}\text{U}$ , IEU, HEU,  $^{239}\text{Pu}$ , and MIX assemblies.

- (1) In these 100 calculation benchmark cases, the calculated values for most of the cases were in good agreement with the experimental values.
- (2) Considering all devices comprehensively and analyzing the values of  $\chi^2$  and  $\langle|\Delta|\rangle$  demonstrates that the overall criticality calculation performance of ENDF/B-VIII.0 and JEFF3.3 is basically equivalent. The ENDF/B-VII.1 library offers the best performance in criticality calculations. In addition, CENDL-3.2 is improved compared to the CENDL-3.1 library and is better than JENDL-4.0. CENDL-3.2 performed better in the calculations of  $^{233}\text{U}$  assemblies. However, for the pusl11 series of Pu devices, CENDL-3.2 has poor performance in criticality calculations and needs further improvement.
- (3) The  $\delta k/\sigma$  values of most benchmark cases in different data libraries were in the  $3\sigma$  interval with a confidence of 99.7%. A few benchmark cases (e.g., 23umet4b, pumet8b, and mixmet8-7) have  $\delta k/\sigma$  values higher than the  $3\sigma$  interval for all libraries. The reason for the large deviation between the calculated value of mixmet8-7 and the experimental value requires further study.

## Appendix

See Tables 8 and 9

**Table 8** ICSBEP benchmark abbreviation and reference  $k_{\text{eff}}$  value

| Type | Abbreviation | ICSBEP reference          | Benchmark $k_{\text{eff}}$ |
|------|--------------|---------------------------|----------------------------|
| 233U | 23umt1       | 233U-MET-FAST-001         | $1.0000 \pm 0.00100$       |
| 233U | 23umt2a      | 233U-MET-FAST-002 Case 1  | $1.0000 \pm 0.00100$       |
| 233U | 23umt2b      | 233U-MET-FAST-002 Case 2  | $1.0000 \pm 0.00110$       |
| 233U | 23umt3a      | 233U-MET-FAST-003 Case 1  | $1.0000 \pm 0.00100$       |
| 233U | 23umt3b      | 233U-MET-FAST-003 Case 2  | $1.0000 \pm 0.00100$       |
| 233U | 23umt4a      | 233U-MET-FAST-004 Case 1  | $1.0000 \pm 0.00070$       |
| 233U | 23umt4b      | 233U-MET-FAST-004 Case 2  | $1.0000 \pm 0.00080$       |
| 233U | 23umt5a      | 233U-MET-FAST-005 Case 1  | $1.0000 \pm 0.00300$       |
| 233U | 23umt5b      | 233U-MET-FAST-005 Case 2  | $1.0000 \pm 0.00300$       |
| 233U | 23umt6       | 233U-MET-FAST-006         | $1.0000 \pm 0.00140$       |
| 233U | 23usl1a      | 233U-SOL-THERM-001 Case 1 | $1.0000 \pm 0.00310$       |
| 233U | 23usl1b      | 233U-SOL-THERM-001 Case 2 | $1.0005 \pm 0.00330$       |
| 233U | 23usl1c      | 233U-SOL-THERM-001 Case 3 | $1.0006 \pm 0.00330$       |
| 233U | 23usl1d      | 233U-SOL-THERM-001 Case 4 | $0.9998 \pm 0.00330$       |
| 233U | 23usl1e      | 233U-SOL-THERM-001 Case 5 | $0.9999 \pm 0.00330$       |
| 233U | 23usl8       | 233U-SOL-THERM-008        | $1.0006 \pm 0.00290$       |
| HEU  | bigten1      | F-10-1 (In CSEWG)         | $0.9960 \pm 0.00300$       |
| HEU  | bigten2      | F-10-2 (In CSEWG)         | $0.9960 \pm 0.00300$       |
| 233U | flat23       | F-24 (In CSEWG)           | $1.0000 \pm 0.00100$       |
| IEU  | ieumt1a      | IEU-MET-FAST-001 Case 1   | $0.9989 \pm 0.00100$       |
| IEU  | ieumt1b      | IEU-MET-FAST-001 Case 2   | $0.9997 \pm 0.00100$       |
| IEU  | ieumt1c      | IEU-MET-FAST-001 Case 3   | $0.9993 \pm 0.00050$       |
| IEU  | ieumt1d      | IEU-MET-FAST-001 Case 4   | $1.0002 \pm 0.00050$       |
| IEU  | ieumt2       | IEU-MET-FAST-002          | $1.0000 \pm 0.00300$       |
| IEU  | ieumt3       | IEU-MET-FAST-003          | $1.0000 \pm 0.00170$       |
| IEU  | ieumt4       | IEU-MET-FAST-004          | $1.0000 \pm 0.00300$       |
| IEU  | ieumt5       | IEU-MET-FAST-005          | $1.0000 \pm 0.00210$       |
| IEU  | ieumt6       | IEU-MET-FAST-006          | $1.0000 \pm 0.00230$       |
| MIX  | mixmet1      | MIX-MET-FAST-001          | $1.0000 \pm 0.00160$       |
| MIX  | mixmet3      | MIX-MET-FAST-001          | $0.9993 \pm 0.00160$       |
| 239U | pumet1       | PU-MET-FAST-001           | $1.0000 \pm 0.00200$       |
| 239U | pumet10      | PU-MET-FAST-010           | $1.0000 \pm 0.00180$       |
| 239U | pumet11      | PU-MET-FAST-011           | $1.0000 \pm 0.00100$       |
| 239U | pumet18      | PU-MET-FAST-018           | $1.0000 \pm 0.00300$       |
| 239U | pumet19      | PU-MET-FAST-019           | $0.9992 \pm 0.00150$       |
| 239U | pumet2       | PU-MET-FAST-002           | $1.0000 \pm 0.00200$       |
| 239U | pumet20      | PU-MET-FAST-020           | $0.9993 \pm 0.00170$       |
| 239U | pumet22      | PU-MET-FAST-022           | $1.0000 \pm 0.00210$       |
| 239U | pumet23      | PU-MET-FAST-023           | $1.0000 \pm 0.00200$       |
| 239U | pumet24      | PU-MET-FAST-024           | $1.0000 \pm 0.00200$       |
| 239U | pumet25      | PU-MET-FAST-025           | $1.0000 \pm 0.00200$       |
| 239U | pumet26      | PU-MET-FAST-026           | $1.0000 \pm 0.00240$       |
| 239U | pumet5       | PU-MET-FAST-005           | $1.0000 \pm 0.00130$       |
| 239U | pumet6       | PU-MET-FAST-006           | $1.0000 \pm 0.00300$       |
| 239U | pumet8a      | PU-MET-FAST-008 Case 1    | $1.0000 \pm 0.00300$       |
| 239U | pumet8b      | PU-MET-FAST-008 Case 2    | $1.0000 \pm 0.00060$       |
| 239U | pumet9       | PU-MET-FAST-009           | $1.0000 \pm 0.00270$       |
| 239U | pumt21a      | PU-MET-FAST-021 Case 1    | $1.0000 \pm 0.00260$       |

Table 8 continued

| Type | Abbreviation | ICSBEP reference              | Benchmark $k_{\text{eff}}$ |
|------|--------------|-------------------------------|----------------------------|
| 239U | pumt21b      | PU-MET-FAST-021 Case 2        | $1.0000 \pm 0.00260$       |
| 239U | pusl11a      | PU-SOL-THERM-011 Case 18–1    | $1.0000 \pm 0.00520$       |
| 239U | pusl11b      | PU-SOL-THERM-011 Case 18–6    | $1.0000 \pm 0.00520$       |
| 239U | pusl11c      | PU-SOL-THERM-011 Case 16–5    | $1.0000 \pm 0.00520$       |
| 239U | pusl11d      | PU-SOL-THERM-011 Case 16–1    | $1.0000 \pm 0.00520$       |
| HEU  | umet11       | HEU-MET-FAST-011              | $0.9989 \pm 0.00150$       |
| HEU  | umet13       | HEU-MET-FAST-013              | $0.9990 \pm 0.00150$       |
| HEU  | umet14       | HEU-MET-FAST-014              | $0.9989 \pm 0.00170$       |
| HEU  | umet18       | HEU-MET-FAST-018              | $1.0000 \pm 0.00160$       |
| HEU  | umet19       | HEU-MET-FAST-019              | $1.0000 \pm 0.00300$       |
| HEU  | umet1ns      | HEU-MET-FAST-001 Case b       | $1.0000 \pm 0.00100$       |
| HEU  | umet1ss      | HEU-MET-FAST-001 Case a       | $1.0000 \pm 0.00100$       |
| HEU  | umet20       | HEU-MET-FAST-020              | $1.0000 \pm 0.00300$       |
| HEU  | umet21       | HEU-MET-FAST-021              | $1.0000 \pm 0.00260$       |
| HEU  | umet22       | HEU-MET-FAST-022              | $1.0000 \pm 0.00210$       |
| HEU  | umet28       | HEU-MET-FAST-028              | $1.0000 \pm 0.00300$       |
| HEU  | umet3a       | HEU-MET-FAST-003 Case 1       | $1.0000 \pm 0.00500$       |
| HEU  | umet3b       | HEU-MET-FAST-003 Case 2       | $1.0000 \pm 0.00500$       |
| HEU  | umet3c       | HEU-MET-FAST-003 Case 3       | $1.0000 \pm 0.00500$       |
| HEU  | umet3d       | HEU-MET-FAST-003 Case 4       | $1.0000 \pm 0.00300$       |
| HEU  | umet3e       | HEU-MET-FAST-003 Case 5       | $1.0000 \pm 0.00300$       |
| HEU  | umet3f       | HEU-MET-FAST-003 Case 6       | $1.0000 \pm 0.00300$       |
| HEU  | umet3g       | HEU-MET-FAST-003 Case 7       | $1.0000 \pm 0.00300$       |
| HEU  | umet3h       | HEU-MET-FAST-003 Case 8       | $1.0000 \pm 0.00500$       |
| HEU  | umet3i       | HEU-MET-FAST-003 Case 9       | $1.0000 \pm 0.00500$       |
| HEU  | umet3j       | HEU-MET-FAST-003 Case 10      | $1.0000 \pm 0.00500$       |
| HEU  | umet3k       | HEU-MET-FAST-003 Case 11      | $1.0000 \pm 0.00500$       |
| HEU  | umet3l       | HEU-MET-FAST-003 Case 12      | $1.0000 \pm 0.00300$       |
| HEU  | umet4a       | HEU-MET-FAST-004 Case 2       | $1.0020 \pm 0.00100$       |
| HEU  | umet4b       | HEU-MET-FAST-004 Case 1       | $1.0003 \pm 0.00050$       |
| HEU  | umet9a       | HEU-MET-FAST-009 Case 1       | $0.9992 \pm 0.00150$       |
| HEU  | umet9b       | HEU-MET-FAST-009 Case 2       | $0.9992 \pm 0.00150$       |
| HEU  | usol13a      | HEU-SOL-THERM-003 Case 1      | $1.0012 \pm 0.00260$       |
| HEU  | usol13b      | HEU-SOL-THERM-003 Case 2      | $1.0007 \pm 0.00360$       |
| HEU  | usol13c      | HEU-SOL-THERM-003 Case 3      | $1.0009 \pm 0.00360$       |
| HEU  | usol13d      | HEU-SOL-THERM-003 Case 4      | $1.0003 \pm 0.00360$       |
| HEU  | usol32       | HEU-SOL-THERM-032             | $1.0015 \pm 0.00260$       |
| HEU  | umet8        | HEU-MET-FAST-008              | $0.9989 \pm 0.00160$       |
| HEU  | umet12       | HEU-MET-FAST-012              | $0.9992 \pm 0.00180$       |
| HEU  | umet15       | HEU-MET-FAST-015              | $0.9996 \pm 0.00170$       |
| MIX  | mixmet8-1    | MIX-MET-FAST-008 Case 1       | $0.9920 \pm 0.00630$       |
| MIX  | mixmet8-7    | MIX-MET-FAST-008 Case 7       | $1.0030 \pm 0.00250$       |
| IEU  | lst7-14      | leu-sol-therm-007-case-14     | $0.9961 \pm 0.00090$       |
| IEU  | lst7-30      | leu-sol-therm-007-case-30     | $0.9973 \pm 0.00090$       |
| IEU  | lst7-32      | leu-sol-therm-007-case-32     | $0.9985 \pm 0.00100$       |
| IEU  | lst7-36      | leu-sol-therm-007-case-36     | $0.9988 \pm 0.00110$       |
| IEU  | lst7-49      | leu-sol-therm-007-case-49     | $0.9983 \pm 0.00110$       |
| MIX  | mct2-pnl30   | mix-comp-therm-002-case-pnl30 | $1.0024 \pm 0.00600$       |

**Table 8** continued

| Type | Abbreviation | ICSBEP reference              | Benchmark $k_{\text{eff}}$ |
|------|--------------|-------------------------------|----------------------------|
| MIX  | mct2-pnl31   | mix-comp-therm-002-case-pnl31 | $1.0009 \pm 0.00470$       |
| MIX  | mct2-pnl33   | mix-comp-therm-002-case-pnl33 | $1.0024 \pm 0.00210$       |
| MIX  | mct2-pnl34   | mix-comp-therm-002-case-pnl34 | $1.0038 \pm 0.00250$       |
| MIX  | mct2-pnl35   | mix-comp-therm-002-case-pnl35 | $1.0029 \pm 0.00270$       |
| MIX  | mmf1         | mix-met-fast-001              | $1.0000 \pm 0.00160$       |
| MIX  | mmf3         | mix-met-fast-003              | $0.9993 \pm 0.00160$       |

**Table 9**  $k_{\text{eff}}$  values and statistical errors of different libraries

| Case    | CENDL-3.1             | CENDL-3.2             | ENDF/B-VII.1          | ENDF/B-VIII.0         | JEFF-3.3              | JENDL-4.0             |
|---------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 23umt1  | $0.99987 \pm 0.00055$ | $1.00211 \pm 0.00058$ | $1.00059 \pm 0.00055$ | $0.99963 \pm 0.00053$ | $1.00080 \pm 0.00056$ | $0.99923 \pm 0.00056$ |
| 23umt2a | $0.99676 \pm 0.00055$ | $0.99936 \pm 0.00059$ | $1.00000 \pm 0.00056$ | $1.00004 \pm 0.00059$ | $0.99955 \pm 0.00057$ | $0.99861 \pm 0.00055$ |
| 23umt2b | $0.99792 \pm 0.00056$ | $1.00111 \pm 0.00056$ | $0.99927 \pm 0.00060$ | $1.00186 \pm 0.00058$ | $1.00183 \pm 0.00061$ | $1.00031 \pm 0.00057$ |
| 23umt3a | $0.99803 \pm 0.00058$ | $1.00014 \pm 0.00060$ | $0.99932 \pm 0.00060$ | $1.00011 \pm 0.00057$ | $1.0022 \pm 0.00060$  | $0.99962 \pm 0.00059$ |
| 23umt3b | $0.99876 \pm 0.00062$ | $0.99996 \pm 0.00059$ | $1.00014 \pm 0.00057$ | $1.00033 \pm 0.00060$ | $1.00206 \pm 0.0006$  | $0.99731 \pm 0.00063$ |
| 23umt4a | $0.99495 \pm 0.00058$ | $1.00034 \pm 0.00058$ | $0.99878 \pm 0.00059$ | $0.99909 \pm 0.00054$ | $1.00038 \pm 0.00060$ | $1.00121 \pm 0.00063$ |
| 23umt4b | $0.99019 \pm 0.00063$ | $0.99711 \pm 0.00061$ | $0.99514 \pm 0.00063$ | $0.99487 \pm 0.00062$ | $0.9982 \pm 0.00063$  | $0.99814 \pm 0.00063$ |
| 23umt5a | $0.99050 \pm 0.00061$ | $0.99517 \pm 0.00061$ | $0.99659 \pm 0.00064$ | $0.99817 \pm 0.00060$ | $0.99698 \pm 0.00062$ | $0.99646 \pm 0.00063$ |
| 23umt5b | $0.98751 \pm 0.00064$ | $0.99441 \pm 0.00063$ | $0.99577 \pm 0.00065$ | $0.99733 \pm 0.00065$ | $0.99612 \pm 0.00065$ | $0.99485 \pm 0.00066$ |
| 23umt6  | $0.99915 \pm 0.00067$ | $0.99901 \pm 0.00070$ | $0.99907 \pm 0.00057$ | $0.99940 \pm 0.00066$ | $1.00359 \pm 0.00068$ | $0.99773 \pm 0.00067$ |
| 23usl1a | $1.00322 \pm 0.00038$ | $1.00128 \pm 0.00036$ | $1.00183 \pm 0.00038$ | $1.00045 \pm 0.00038$ | $1.00209 \pm 0.00038$ | $0.99770 \pm 0.00039$ |
| 23usl1b | $1.00333 \pm 0.00039$ | $1.00109 \pm 0.00037$ | $1.00224 \pm 0.00039$ | $1.00005 \pm 0.00037$ | $1.00162 \pm 0.00040$ | $0.99775 \pm 0.00038$ |
| 23usl1c | $1.00243 \pm 0.00038$ | $1.00006 \pm 0.00039$ | $1.00147 \pm 0.00040$ | $1.00027 \pm 0.00038$ | $1.00157 \pm 0.00039$ | $0.99746 \pm 0.00039$ |
| 23usl1d | $1.00243 \pm 0.00039$ | $1.00041 \pm 0.00039$ | $1.00162 \pm 0.00037$ | $0.99976 \pm 0.00039$ | $1.00098 \pm 0.00042$ | $0.99730 \pm 0.00040$ |
| 23usl1e | $1.00185 \pm 0.00040$ | $1.00033 \pm 0.00042$ | $1.00037 \pm 0.00041$ | $0.99906 \pm 0.00039$ | $1.00135 \pm 0.00042$ | $0.99644 \pm 0.00040$ |
| 23usl8  | $1.00131 \pm 0.00026$ | $0.99988 \pm 0.00025$ | $1.00129 \pm 0.00025$ | $0.99976 \pm 0.00026$ | $1.00214 \pm 0.00025$ | $0.99680 \pm 0.00026$ |
| bigten1 | $0.99801 \pm 0.00048$ | $0.99649 \pm 0.00052$ | $0.99823 \pm 0.00047$ | $0.99667 \pm 0.00048$ | $0.99862 \pm 0.00051$ | $0.99023 \pm 0.00047$ |
| bigten2 | $0.99613 \pm 0.00047$ | $0.99385 \pm 0.00049$ | $0.99628 \pm 0.00048$ | $0.99644 \pm 0.00049$ | $0.99693 \pm 0.00049$ | $0.98773 \pm 0.00044$ |
| flat23  | $1.00027 \pm 0.00064$ | $1.00138 \pm 0.00064$ | $1.00032 \pm 0.00066$ | $1.00291 \pm 0.00065$ | $1.00512 \pm 0.00067$ | $0.99920 \pm 0.00066$ |
| ieumt1a | $1.00007 \pm 0.00061$ | $1.00039 \pm 0.00061$ | $1.00109 \pm 0.00056$ | $0.99864 \pm 0.00057$ | $0.99978 \pm 0.00058$ | $0.99673 \pm 0.00058$ |
| ieumt1b | $1.00140 \pm 0.00061$ | $1.00102 \pm 0.00061$ | $1.00061 \pm 0.00056$ | $0.99946 \pm 0.00060$ | $1.00086 \pm 0.00058$ | $0.99644 \pm 0.00060$ |
| ieumt1c | $1.00277 \pm 0.00061$ | $0.99941 \pm 0.00058$ | $1.00158 \pm 0.00060$ | $0.99893 \pm 0.00059$ | $1.00000 \pm 0.00058$ | $0.99521 \pm 0.00060$ |
| ieumt1d | $1.00141 \pm 0.00061$ | $1.00081 \pm 0.00059$ | $1.00188 \pm 0.00058$ | $0.99856 \pm 0.00063$ | $1.00022 \pm 0.00061$ | $0.99483 \pm 0.00058$ |
| ieumt2  | $0.99818 \pm 0.00059$ | $0.99884 \pm 0.00052$ | $0.99925 \pm 0.00058$ | $0.99610 \pm 0.00052$ | $0.99620 \pm 0.00055$ | $0.98842 \pm 0.00057$ |
| ieumt3  | $1.00123 \pm 0.00060$ | $1.00138 \pm 0.00057$ | $1.00261 \pm 0.00062$ | $0.99898 \pm 0.00061$ | $1.00147 \pm 0.00057$ | $0.99598 \pm 0.00061$ |
| ieumt4  | $1.00838 \pm 0.00060$ | $1.00672 \pm 0.00059$ | $1.00749 \pm 0.00059$ | $1.00529 \pm 0.00061$ | $1.00543 \pm 0.00062$ | $0.99869 \pm 0.00061$ |
| ieumt5  | $1.00015 \pm 0.00055$ | $1.00467 \pm 0.00061$ | $1.00131 \pm 0.00056$ | $1.00044 \pm 0.00065$ | $1.00048 \pm 0.00060$ | $0.99469 \pm 0.00054$ |
| ieumt6  | $0.99812 \pm 0.00060$ | $0.99560 \pm 0.00054$ | $0.99677 \pm 0.00059$ | $0.99397 \pm 0.00055$ | $0.99335 \pm 0.00058$ | $0.99003 \pm 0.00058$ |
| mixmet1 | $0.99905 \pm 0.00059$ | $0.9984 \pm 0.00058$  | $1.00009 \pm 0.00058$ | $0.99891 \pm 0.00057$ | $0.99858 \pm 0.00055$ | $0.99774 \pm 0.00056$ |
| mixmet3 | $0.9999 \pm 0.000610$ | $1.00074 \pm 0.00062$ | $1.00084 \pm 0.00064$ | $1.00087 \pm 0.00066$ | $1.00030 \pm 0.00062$ | $0.99795 \pm 0.00058$ |
| pumet1  | $1.00253 \pm 0.00055$ | $1.00218 \pm 0.00058$ | $1.00031 \pm 0.00056$ | $1.00008 \pm 0.00058$ | $0.99953 \pm 0.00058$ | $0.99878 \pm 0.00060$ |
| pumet10 | $0.99852 \pm 0.00060$ | $0.99848 \pm 0.00060$ | $0.99966 \pm 0.00060$ | $0.99797 \pm 0.00060$ | $1.00002 \pm 0.00062$ | $0.99628 \pm 0.00059$ |
| pumet11 | $1.00243 \pm 0.00079$ | $1.00094 \pm 0.00074$ | $0.99953 \pm 0.00071$ | $0.99955 \pm 0.00068$ | $1.00056 \pm 0.00073$ | $1.00137 \pm 0.00070$ |
| pumet18 | $0.99854 \pm 0.00061$ | $0.99652 \pm 0.00061$ | $1.00024 \pm 0.00065$ | $0.99828 \pm 0.00061$ | $0.99804 \pm 0.00061$ | $0.99760 \pm 0.00060$ |
| pumet2  | $1.00234 \pm 0.00058$ | $1.00304 \pm 0.00059$ | $1.00050 \pm 0.00057$ | $1.00126 \pm 0.00057$ | $1.00216 \pm 0.00058$ | $0.99794 \pm 0.00059$ |
| pumet20 | $0.99561 \pm 0.00064$ | $0.99738 \pm 0.00064$ | $0.99814 \pm 0.00061$ | $0.99664 \pm 0.00061$ | $0.99942 \pm 0.00056$ | $0.99616 \pm 0.00063$ |
| pumet22 | $1.00061 \pm 0.00057$ | $0.99995 \pm 0.00054$ | $0.99924 \pm 0.00057$ | $0.99859 \pm 0.00057$ | $0.99772 \pm 0.00056$ | $0.99624 \pm 0.00054$ |

Table 9 continued

| Case    | CENDL-3.1         | CENDL-3.2         | ENDF/B-VII.1      | ENDF/B-VIII.0     | JEFF-3.3          | JENDL-4.0         |
|---------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| pumet23 | 1.00001 ± 0.00061 | 1.00098 ± 0.00057 | 0.99935 ± 0.00058 | 0.99717 ± 0.00059 | 1.00003 ± 0.00054 | 0.99556 ± 0.00061 |
| pumet24 | 1.00367 ± 0.00064 | 1.00362 ± 0.00065 | 1.00124 ± 0.00063 | 1.00128 ± 0.00064 | 1.00100 ± 0.00061 | 1.00023 ± 0.00062 |
| pumet25 | 0.99696 ± 0.00058 | 1.00024 ± 0.00060 | 0.99992 ± 0.00057 | 1.00056 ± 0.00062 | 0.99662 ± 0.00060 | 0.99651 ± 0.00059 |
| pumet26 | 0.99313 ± 0.00057 | 1.00042 ± 0.00061 | 0.99969 ± 0.00060 | 1.00077 ± 0.00058 | 0.99759 ± 0.00064 | 0.99486 ± 0.00062 |
| pumet5  | 1.00024 ± 0.00057 | 1.00165 ± 0.00061 | 1.00176 ± 0.00063 | 0.99948 ± 0.00061 | 1.00113 ± 0.00064 | 1.00200 ± 0.00061 |
| pumet6  | 0.99877 ± 0.00061 | 0.99832 ± 0.00070 | 0.99996 ± 0.00071 | 0.99918 ± 0.00074 | 1.00354 ± 0.00067 | 0.99947 ± 0.00069 |
| pumet8a | 1.00371 ± 0.00059 | 1.00254 ± 0.00059 | 0.99807 ± 0.00061 | 0.99753 ± 0.00061 | 0.99801 ± 0.00062 | 0.99747 ± 0.00062 |
| pumet8b | 1.00367 ± 0.00062 | 1.00292 ± 0.00061 | 0.99778 ± 0.00063 | 0.99677 ± 0.00054 | 0.99683 ± 0.00060 | 0.99644 ± 0.00062 |
| pumet9  | 1.00483 ± 0.00058 | 1.01041 ± 0.00061 | 1.00577 ± 0.00063 | 1.00511 ± 0.00063 | 1.00437 ± 0.00059 | 1.00183 ± 0.00057 |
| pumt21b | 0.99428 ± 0.00060 | 0.99490 ± 0.00062 | 0.99372 ± 0.00064 | 0.99176 ± 0.00063 | 0.99332 ± 0.00064 | 0.99422 ± 0.00066 |
| pusl11a | 1.01086 ± 0.00052 | 1.00619 ± 0.00054 | 0.99577 ± 0.00051 | 0.98934 ± 0.00055 | 0.99104 ± 0.0005  | 0.99605 ± 0.00052 |
| pusl11b | 1.01542 ± 0.00053 | 1.01321 ± 0.00054 | 1.00147 ± 0.00055 | 0.99524 ± 0.00054 | 0.99601 ± 0.00055 | 1.00078 ± 0.00055 |
| pusl11c | 1.02311 ± 0.00062 | 1.01914 ± 0.00062 | 1.00528 ± 0.00063 | 0.99987 ± 0.00062 | 1.0025 ± 0.00060  | 1.00659 ± 0.00060 |
| pusl11d | 1.02745 ± 0.00061 | 1.02445 ± 0.00059 | 1.00898 ± 0.00060 | 1.00400 ± 0.00060 | 1.00645 ± 0.00058 | 1.01147 ± 0.00061 |
| umet11  | 0.99985 ± 0.00072 | 0.99868 ± 0.00069 | 0.99752 ± 0.00074 | 0.99657 ± 0.00070 | 0.99732 ± 0.00073 | 0.99465 ± 0.00077 |
| umet13  | 0.99589 ± 0.00060 | 0.99865 ± 0.00063 | 0.99829 ± 0.00059 | 0.99839 ± 0.00058 | 0.99630 ± 0.00059 | 0.99381 ± 0.00060 |
| umet14  | 0.99665 ± 0.00060 | 0.99767 ± 0.00062 | 0.99842 ± 0.00057 | 0.99588 ± 0.00063 | 0.99818 ± 0.00063 | 0.99341 ± 0.00058 |
| umet18  | 0.99958 ± 0.00059 | 0.99902 ± 0.00059 | 0.99972 ± 0.00054 | 0.99985 ± 0.00059 | 1.00025 ± 0.00062 | 0.99680 ± 0.00056 |
| umet19  | 1.00921 ± 0.00061 | 1.00776 ± 0.00065 | 1.00676 ± 0.00063 | 1.00526 ± 0.00060 | 1.00683 ± 0.0006  | 1.00086 ± 0.00061 |
| umet1ns | 1.00107 ± 0.00057 | 0.99983 ± 0.00054 | 1.00009 ± 0.00060 | 1.00075 ± 0.00056 | 1.00028 ± 0.00058 | 0.99886 ± 0.00057 |
| umet1ss | 1.00098 ± 0.00057 | 1.00064 ± 0.00054 | 1.00043 ± 0.00057 | 1.00004 ± 0.00057 | 1.00085 ± 0.00055 | 0.99806 ± 0.00055 |
| umet20  | 1.00135 ± 0.00063 | 1.00088 ± 0.00066 | 0.99999 ± 0.00066 | 0.99955 ± 0.00065 | 1.00062 ± 0.00063 | 0.99699 ± 0.00063 |
| umet21  | 0.99525 ± 0.00061 | 1.00066 ± 0.00062 | 0.99820 ± 0.00063 | 0.99916 ± 0.00065 | 0.99765 ± 0.00058 | 0.99370 ± 0.00057 |
| umet22  | 0.99777 ± 0.00057 | 0.99934 ± 0.00059 | 0.99677 ± 0.00057 | 0.99763 ± 0.00058 | 0.99719 ± 0.00060 | 0.99428 ± 0.00056 |
| umet28  | 1.00207 ± 0.00061 | 1.00103 ± 0.00064 | 1.00443 ± 0.00062 | 0.99940 ± 0.00061 | 1.00363 ± 0.00058 | 0.99690 ± 0.00063 |
| umet3a  | 0.99528 ± 0.00062 | 0.99435 ± 0.00062 | 0.99457 ± 0.00065 | 0.99281 ± 0.00055 | 0.99706 ± 0.00058 | 0.99083 ± 0.00062 |
| umet3b  | 0.99281 ± 0.00060 | 0.99275 ± 0.00058 | 0.99341 ± 0.00058 | 0.99221 ± 0.00061 | 0.99574 ± 0.00059 | 0.98881 ± 0.00058 |
| umet3c  | 0.99888 ± 0.00061 | 0.99928 ± 0.00062 | 0.99988 ± 0.00062 | 0.99672 ± 0.00062 | 0.99905 ± 0.00062 | 0.99427 ± 0.00064 |
| umet3d  | 0.99544 ± 0.00063 | 0.99557 ± 0.00060 | 0.99668 ± 0.00061 | 0.99581 ± 0.00065 | 0.99797 ± 0.00066 | 0.99183 ± 0.00062 |
| umet3e  | 1.00020 ± 0.00064 | 0.99973 ± 0.00063 | 1.00160 ± 0.00060 | 0.99861 ± 0.00064 | 1.00200 ± 0.00059 | 0.99487 ± 0.00062 |
| umet3f  | 1.0003 ± 0.00067  | 1.00028 ± 0.00062 | 1.00016 ± 0.00059 | 0.99824 ± 0.00061 | 1.0027 ± 0.00065  | 0.99583 ± 0.00065 |
| umet3g  | 1.00099 ± 0.00063 | 1.00051 ± 0.00065 | 1.00320 ± 0.00061 | 0.99938 ± 0.00065 | 1.00373 ± 0.00058 | 0.99678 ± 0.00066 |
| umet3h  | 1.00010 ± 0.00057 | 1.00234 ± 0.00061 | 1.00107 ± 0.00064 | 0.99986 ± 0.00062 | 1.00175 ± 0.00063 | 0.99751 ± 0.00064 |
| umet3i  | 1.00145 ± 0.00060 | 1.00207 ± 0.00063 | 1.00162 ± 0.00060 | 0.99928 ± 0.00063 | 1.00108 ± 0.00063 | 0.99842 ± 0.00060 |
| umet3j  | 1.00367 ± 0.00064 | 1.00586 ± 0.00063 | 1.00482 ± 0.00061 | 1.00333 ± 0.00064 | 1.00527 ± 0.00062 | 1.00106 ± 0.00059 |
| umet3k  | 1.00929 ± 0.00065 | 1.01174 ± 0.00059 | 1.00967 ± 0.00061 | 1.00814 ± 0.00059 | 1.00831 ± 0.00057 | 1.00676 ± 0.00066 |
| umet3l  | 0.99675 ± 0.00062 | 0.99581 ± 0.00058 | 1.00772 ± 0.00065 | 0.99902 ± 0.00061 | 1.00432 ± 0.00060 | 1.00180 ± 0.00061 |
| umet4a  | 1.00455 ± 0.00071 | 1.00382 ± 0.00074 | 1.00416 ± 0.00073 | 1.00243 ± 0.00074 | 1.00081 ± 0.00071 | 1.00280 ± 0.00074 |
| umet4b  | 1.00101 ± 0.00072 | 0.99773 ± 0.00071 | 0.99912 ± 0.00071 | 0.99637 ± 0.00077 | 0.99796 ± 0.00074 | 0.99884 ± 0.00071 |
| umet9a  | 0.99743 ± 0.00064 | 0.99560 ± 0.00062 | 0.99765 ± 0.00060 | 0.99695 ± 0.00060 | 0.99657 ± 0.00068 | 0.99400 ± 0.00060 |
| umet9b  | 0.99616 ± 0.00061 | 0.99479 ± 0.00062 | 0.99669 ± 0.00065 | 0.99649 ± 0.00062 | 0.99558 ± 0.00060 | 0.99395 ± 0.00060 |
| usol13a | 1.00173 ± 0.00038 | 0.99731 ± 0.00039 | 0.99923 ± 0.00039 | 0.99930 ± 0.00037 | 0.99722 ± 0.00037 | 0.99951 ± 0.00037 |
| usol13b | 1.00024 ± 0.00041 | 0.99628 ± 0.00040 | 0.99850 ± 0.00039 | 0.99873 ± 0.00042 | 0.99784 ± 0.00040 | 0.99718 ± 0.00040 |
| usol13c | 0.99653 ± 0.00043 | 0.99211 ± 0.00043 | 0.99390 ± 0.00041 | 0.99550 ± 0.00040 | 0.99440 ± 0.00042 | 0.99404 ± 0.00043 |
| usol13d | 0.99747 ± 0.00041 | 0.99408 ± 0.00045 | 0.99492 ± 0.00044 | 0.99660 ± 0.00044 | 0.99536 ± 0.00041 | 0.99614 ± 0.00042 |
| usol32  | 1.00082 ± 0.00025 | 0.99666 ± 0.00024 | 0.99890 ± 0.00025 | 0.99893 ± 0.00024 | 0.99742 ± 0.00025 | 0.99894 ± 0.00025 |
| umet8   | 0.99632 ± 0.00054 | 0.99645 ± 0.00061 | 0.99577 ± 0.00059 | 0.99584 ± 0.00057 | 0.99497 ± 0.00059 | 0.99401 ± 0.00054 |

**Table 9** continued

| Case       | CENDL-3.1         | CENDL-3.2         | ENDF/B-VII.1      | ENDF/B-VIII.0     | JEFF-3.3          | JENDL-4.0         |
|------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| umet12     | 0.99977 ± 0.00057 | 1.00007 ± 0.00054 | 0.99814 ± 0.00062 | 0.99779 ± 0.00057 | 0.99733 ± 0.00062 | 0.99639 ± 0.00059 |
| umet15     | 0.99453 ± 0.00055 | 0.99520 ± 0.00059 | 0.99436 ± 0.00057 | 0.99499 ± 0.00052 | 0.99435 ± 0.00057 | 0.99367 ± 0.00059 |
| mixmet8-1  | 0.99477 ± 0.00048 | 0.99607 ± 0.00047 | 0.99526 ± 0.00048 | 0.99584 ± 0.00057 | 0.99497 ± 0.00059 | 0.99401 ± 0.00054 |
| mixmet8-7  | 1.02400 ± 0.00016 | 1.02087 ± 0.00018 | 1.01920 ± 0.00018 | 1.02361 ± 0.00020 | 1.02653 ± 0.00017 | 1.01691 ± 0.00017 |
| lst7-14    | 0.99894 ± 0.00030 | 0.99479 ± 0.00031 | 0.99726 ± 0.00029 | 0.99831 ± 0.00031 | 0.99756 ± 0.00029 | 0.99449 ± 0.00031 |
| lst7-30    | 0.99894 ± 0.00030 | 0.99479 ± 0.00031 | 0.99726 ± 0.00029 | 0.99831 ± 0.00031 | 0.99756 ± 0.00029 | 0.99449 ± 0.00031 |
| lst7-32    | 0.99786 ± 0.00030 | 0.99492 ± 0.00029 | 0.99559 ± 0.00029 | 0.99694 ± 0.00029 | 0.99587 ± 0.00027 | 0.99389 ± 0.00031 |
| lst7-36    | 1.00039 ± 0.00026 | 0.99717 ± 0.00028 | 0.99900 ± 0.00027 | 0.99975 ± 0.00027 | 0.99910 ± 0.00026 | 0.99596 ± 0.00027 |
| lst7-49    | 0.99887 ± 0.00028 | 0.99566 ± 0.00028 | 0.99721 ± 0.00027 | 0.99844 ± 0.00027 | 0.99752 ± 0.00027 | 0.99429 ± 0.00026 |
| mct2-pnl30 | 1.00157 ± 0.00034 | 1.00000 ± 0.00035 | 0.99939 ± 0.00034 | 0.99825 ± 0.00032 | 1.00103 ± 0.00033 | 1.00170 ± 0.00034 |
| mct2-pnl31 | 1.00374 ± 0.00078 | 1.00357 ± 0.00079 | 1.00296 ± 0.00084 | 1.00315 ± 0.00071 | 1.00482 ± 0.00076 | 1.00558 ± 0.00078 |
| mct2-pnl33 | 1.00846 ± 0.00034 | 1.00733 ± 0.00034 | 1.00694 ± 0.00035 | 1.00455 ± 0.00032 | 1.00514 ± 0.00032 | 1.00878 ± 0.00036 |
| mct2-pnl34 | 1.00831 ± 0.00031 | 1.00686 ± 0.00031 | 1.00239 ± 0.00033 | 1.00101 ± 0.00032 | 1.00161 ± 0.00033 | 1.00409 ± 0.00034 |
| mct2-pnl35 | 1.00756 ± 0.00034 | 1.00697 ± 0.00033 | 1.00572 ± 0.00033 | 1.00395 ± 0.00032 | 1.00431 ± 0.00033 | 1.00816 ± 0.00031 |
| mmf1       | 0.99888 ± 0.00027 | 0.99905 ± 0.00026 | 0.99993 ± 0.00026 | 0.99961 ± 0.00026 | 0.99848 ± 0.00026 | 0.99773 ± 0.00027 |
| mmf3       | 1.00056 ± 0.00028 | 1.00068 ± 0.00027 | 1.00083 ± 0.00029 | 1.00104 ± 0.00027 | 1.00039 ± 0.00027 | 0.99943 ± 0.00028 |

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