

EFFECT OF HEATING RATE ON NONLINEARITY OF DOSE RESPONSE IN TL BY KINETICS MODEL*

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ABSTRACT

The general-order kinetics model of thermoluminescence is used to study the effect of heating rate on the nonlinearity of dose response in thermoluminescence. The results show that when we consider the dose dependence of the maximum intensity of the glow peak, the effect of the heating process on dose response is supralinear when the order of kinetics $b > 1$, and this effect is enhanced with the increase in heating rate.

Keywords Thermoluminescence, Heating rate, Kinetics model, Dose response

1 INTRODUCTION

When considering the dose dependence of the area under the glow curve of thermoluminescence (TL), it is well known that the dose response function $f(D)$ of TL is highly dependent on both the ionization density, i.e. the linear energy transfer (LEF) of the incident radiation, and the nature of the host material. Moreover, when we consider the dose dependence of the maximum intensity of glow curve I_m , due to that the shape of glow curve depends on the heating process, $f(D)$ depends also on the heating process. There are experimental results which show that the nonlinearity of $f(D)$ is increased with the heating rate^[1,2]. Using the second-order kinetics model, one can expect that I_m varies with the dose D as D^p where p slightly exceeds unity ($1.05 \leq p \leq 1.10$)^[3], which shows immediately that I_m varies slightly supralinearly with the dose D , but the effect of heating rate on the dose response is not given. In this paper, the general-order kinetics model of TL will be used to study this effect theoretically.

2 MATHEMATICS ANALYSIS AND RESULTS

For the convenience of analysing the effects of the heating rate on the dose response, the dose response function $f(D)$ is defined as

$$f(D) = [dI_m/dD]/[dI_{mL}/dD_L] \quad (1)$$

where I_{mL} is the maximum TL intensity at a referring dose D_L which is in low dose range. This dose response function $f(D)$ can be divided into two parts as

* Work supported in part by the Foundation of Zhongshan University Advanced Research Center

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Manuscript received date: 1994-08-05

$$f(D) = f_s(D) \cdot f_h(n_0) \quad (2)$$

where

$$f_s(D) = [dn_o/dD]/[dn_{oL}/dD_L] \quad \text{and} \quad f_h(n_0) = [dI_m/dn_o]/[dI_{mL}/dn_{oL}] \quad (3)$$

where n_0 is the initial concentration of trapped carriers and when dose is equal to D_L , we denote it by n_{oL} . The $f_s(D)$ which is related to the dose dependence of the initial concentration of trapped carriers does not depend on the heating rate, so it will not be discussed in this paper. We will focus our attention to the $f_h(n_0)$ which is related to the heating rate.

The glow intensity for a general-order kinetics for a linear heating rate is given by^[4]

$$I = sn_0^b \exp(-E/KT) \left\{ \frac{(b-1)}{\beta} sn_0^{b-1} F(T) + 1 \right\}^{-b/(b-1)} \quad (4)$$

and the maximum condition is

$$\frac{(b-1)sn_0^{b-1}}{\beta} F(T_m) + 1 = \frac{sn_0^{b-1}bKT_m^2}{\beta E} \exp(-E/KT_m) \quad (5)$$

where

$$F(T) = \int_{T_0}^T \exp(-E/KT') dT'$$

s is a pre-exponential factor, E is the activation energy, K is Boltzmann's constant, T_m is the temperature at the maximum, β is the heating rate and b is the order of kinetics. It is well known that $F(T)$ can be replaced by an asymptotic series^[5]

$$F(T) = T \exp(-E/KT) \sum_{n=1}^{\infty} (-1)^{n-1} n! (KT/E)^n \quad (6)$$

Taking derivatives of equation(5) with respect to n_0 and β respectively and expanding them into power series of KT_m/E , one can get the expressions

$$dT_m/d\beta = [KT_m^2/E\beta] \left\{ 1 - KT_m/E + (6-2b)(KT_m/E)^2 + \dots \right\} \quad (7)$$

and

$$\frac{dT_m}{dn_0} = -(b-1) \frac{KT_m^2}{En_0} \left\{ 1 - \frac{KT_m}{E} + (6-2b) \left(\frac{KT_m}{E} \right)^2 + \dots \right\} \quad (8)$$

Using equations (4), (5), (6) and (8), one can get

$$dI_m/dn_0 = [C\beta E/KT_m^2] \left\{ 1 + 2bKT_m/E - 4(KT_m/E)^2 + \dots \right\} \quad (9)$$

where C is a constant.

Inserting Eq.(9) to Eq.(3), and expanding it into power series of KT_m/E and KT_{mL}/E , one has

$$f_h(n_0) = \frac{T_{mL}^2}{T_m^2} \left\{ 1 + 2b \frac{K}{E} (T_m - T_{mL}) + 4 \left(\frac{K}{E} \right)^2 (T_{mL}^2 - T_m^2) + 4b^2 \left(\frac{KT_{mL}}{E} \right)^2 + \dots \right\} \quad (10)$$

where T_{mL} is the temperature at the maximum referring to the dose D_L . Noting that $E \gg KT_m$ in general, the value of E is typically around $20KT_m$, by only keeping the first term of equations, we can derive approximately

$$dT_m/d\beta = KT_m^2/E\beta \quad (11)$$

$$dT_m/dn_0 = -(b-1)KT_m^2/En_0 \quad (12)$$

$$f_h(n_0) = T_{mL}^2/T_m^2 \quad (13)$$

and

$$df_h(n_0)/d\beta = (2KT_{mL}^2/\beta ET_m^2)(T_{mL} - T_m) \quad (14)$$

3 DISCUSSIONS

In the present work, the general-order kinetics model is used to theoretically study the effects of the heating rate on the nonlinearity of dose response in TL. The expression of the dose response to the heating rate is deduced based on the general-order kinetics. From Eqs.(11) and (12), one can see that the temperature T_m increases with the heating rate β and the change of T_m with the initial concentration of trapped carriers n_0 is dependent on the order of kinetics b . For $b > 1$, T_m decreases with increasing n_0 ; for $b < 1$, T_m increases with n_0 ; and for $b = 1$, T_m will not change. Equation (13) shows that $f_h(n_0)$, which is the part of the dose response function relating to the heating rate, is inversely proportional to T_m^2 . Thus for $b > 1$, $b < 1$ and $b = 1$, $f_h(n_0)$ is supralinear, sublinear, and equal to 1 respectively according to the kinetics model. It can also be seen from Eq.(14) that these effects are more obvious for larger heating rates.

In general, the order of kinetics b is assumed to be larger than 1. In this case, from the above discussions, one comes to the conclusion that the effect of heating rate on the dose response is supralinear, and this effect is enhanced with the increase in heating rate, which is in agreement with experimental results.

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